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**EUROCONTROL EXPERIMENTAL CENTRE**

**USER MANUAL FOR  
THE BASE OF AIRCRAFT DATA (BADA)  
REVISION 3.0**

**EEC Note No. 6/98**

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**User Manual  
for the  
Base of Aircraft Data (BADA)  
Revision 3.0**

EUROCONTROL Experimental Centre

Summary

The Base of Aircraft Data (BADA) provides a set of ASCII files containing performance and operating procedure coefficients for 151 different aircraft types. The coefficients include those used to calculate thrust, drag and fuel flow and those used to specify nominal cruise, climb and descent speeds. The User Manual for Revision 3.0 of BADA provides definitions of each of the coefficients and then explains the file formats. Instructions for remotely accessing the files via Internet are also given.

## User Manual Modification History

Issue Number	Release Date	Comments
Revision 2.1 Issue 1.0	31.05.94	First release of document
Revision 2.2 Issue 1.0	25.01.95	<p>Released with BADA Revision 2.2</p> <ul style="list-style-type: none"> <li>- 8 new aircraft models</li> <li>- 2 modified aircraft models</li> <li>- 2 modified equivalences</li> <li>- 6 removed equivalences</li> <li>- 14 new equivalences</li> <li>- modified file formats</li> <li>- additional Synonym File</li> <li>- corrections to formulas in previous version of document</li> <li>- additional description of total-energy and standard atmosphere equations</li> </ul>
Revision 2.3 Issue 1.0	08.06.95	<p>Released with BADA Revision 2.3</p> <ul style="list-style-type: none"> <li>- document format modified to be consistent with EEC Technical Note standards</li> <li>- new A/C models for B73V and D328</li> <li>- MD11 changed from equivalence to direct support</li> <li>- generic military fighter model, FGTR, replaces specific fighter models</li> <li>- maximum payload parameter added to all OPF files</li> <li>- Performance Tables Files (*.PTF) introduced</li> <li>- ISA equations used for TAS/CAS conversions instead of approximations (Section 3.2)</li> <li>- use only one formula for correction of speeds at mass values different from reference mass (Section 3.3)</li> <li>- add specification of minimum speed as function of stall speed (Section 3.4)</li> <li>- specification of transition altitude calculated added (Section 4.1)</li> <li>- speed schedules modified for climb (Section 4.1) and descent (Section 4.3)</li> <li>- modify Internet address for remote access and Eurocontrol contact person (Section 6)</li> <li>- removed Section 7 (General Comments)</li> </ul>

## User Manual Modification History (cont'd)

Issue Number	Release Date	Comments
Revision 2.4 Issue 1.0	04.01.96	<p>Released with BADA Revision 2.4</p> <ul style="list-style-type: none"> <li>- new A/C model for FK70</li> <li>- C421 changed from equivalence to directly supported</li> <li>- 10 new equivalences</li> <li>- 1 modified equivalence</li> <li>- 3 re-developed models</li> <li>- introduction of dynamic maximum altitude</li> <li>- new temperature correction on thrust</li> <li>- modified max.alt for 4 models</li> <li>- modified minimum weight for 2 models</li> <li>- modified temperature coefficients for 12 models</li> <li>- esf calculation for constant CAS below tropopause changed from binomial approximation to exact formula</li> <li>- cruise Mach numbers changed for 4 models</li> <li>- change in altitude limit for descent speed</li> </ul>
Revision 2.5 Issue 1.0	20.01.97	<ul style="list-style-type: none"> <li>- re-developed models: EA32, B737, B73S, AT42, B767, DC9, BA46, FK10, MD80.</li> <li>- new model: CL65, DH83</li> <li>- change of minimum speeds</li> <li>- change of climb/descent speed schedules</li> <li>- cruise fuel flow correction</li> <li>- buffeting speed for jet a/c</li> <li>- addition of BADA.GPF file</li> <li>- definition of acceleration limits, bank angles and holding speeds</li> <li>- 38 new equivalences added (SA4, SA5, SweDen 96)</li> <li>- 1 modified equivalence (B74S)</li> <li>- modified climb/cruise speeds (BE90, BE99, E120, PA42, FK50, B73F, B767, B747, B727, DA20)</li> <li>- Format changes in OPF file</li> <li>- Header changes in PTF file</li> <li>- Temperature influence on thrust limitation changed</li> <li>- Unit of Vstall in OPF file changed to KCAS</li> <li>- Correction of typing errors</li> <li>- Correction of APF file format explanation</li> </ul>

## User Manual Modification History (cont'd)

Issue Number	Release Date	Comments
Revision 2.6 Issue 1.0	01.09..97	<ul style="list-style-type: none"> <li>- Added non-clean drag and thrust data for: EA32, B73S, MD80, B737, B747, FK10, AT42, B767 and CL65 models</li> <li>- All models mentioned above were re-developed using new clean drag data.</li> <li>- ND16, E120 and FK50 were re-modelled to correct the cruise speed capability.</li> <li>- Change of speed schedule in the take-off / initial climb phase and approach / landing phase</li> <li>- Change in descent thrust algorithm</li> <li>- Use of exact formula for density below tropopause instead of approximation.</li> <li>- Addition of formula for pressure above tropopause</li> <li>- Change of buffeting limit to 1.2g (was 1.3g)</li> <li>- Change of OPF file format</li> <li>- Buffeting coefficients for B757 and MD80 were corrected.</li> <li>- Hmo for B747 model was corrected to 45,000 ft</li> <li>- Low altitude descent behaviour corrected for: SW3, PAYE, DA50, DA10, D328, C421, BE99, BE20 and BE90 models</li> <li>- Correction of some minor typing errors</li> <li>- dynamic maximum altitude coefficients changed for B747, B74F, C130 and EA30</li> <li>- Saab 2000 (SB20) added as equivalent of D328</li> <li>- Modified algorithm for liftcoefficient</li> </ul>
Revision 3.0 Issue 1.0	1-3-98	<ul style="list-style-type: none"> <li>- Climb speed law changed for jet aircraft</li> <li>- Descent speed law changed for jet, turbo and piston</li> <li>- Reduced power climbs</li> <li>- B777, SB20 and B73X models were added</li> <li>- DA01 model was removed</li> <li>- Use of ICAO doc. 8643/25 standard, which resulted in the removal of 4 additional models</li> <li>- B73F and B757 remodelled</li> <li>- MD90 added as equivalenced model</li> <li>- Cruise and descent speeds for several turboprops changed</li> <li>- Climb thrust for several a/c changed</li> <li>- Removal of <math>C_{m16}</math> from drag expression</li> </ul>

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**APPENDIX A:****BADA 3.0 - RELEASE SUMMARY FILE****APPENDIX B:****BADA 3.0 - TAR FILE CONTENTS****APPENDIX C:****BADA 3.0 - LIST OF AVAILABLE AIRCRAFT MODELS**

# 1. INTRODUCTION

## 1.1 Identification

This document is the User Manual for the Base of Aircraft Data (BADA) Revision 3.0. This manual replaces the previous User Manual for BADA Revision 2.6 [RD1].

## 1.2 Purpose

BADA is a collection of ASCII files which specifies operation performance parameters, airline procedure parameters and performance summary tables for 151 aircraft types. This information is designed for use in trajectory simulation and prediction algorithms within the domain of Air Traffic Management (ATM). All files are maintained within a configuration management system at the Eurocontrol Experimental Centre (EEC) in Brétigny-sur-Orge, France.

This document describes the mathematical models on which the data is based and specifies the format of the files which contain the data. In addition, this document describes how the files can be remotely accessed from the EEC.

## 1.3 Document Organisation

This document consists of seven sections including Section 1, the Introduction. A list of referenced documents along with a glossary of acronyms and symbols are included in this section.

Section 2, Revision Summary, provides a list of the aircraft types supported by BADA 3.0 and summarises the differences between BADA 3.0 and the previous revision BADA 2.6.

Section 3, Operation Performance Models, defines the set of equations which are used to parameterise aircraft performance. This includes models of aerodynamic drag, engine thrust, and fuel consumption.

Section 4, Airline Procedure Models, defines the set of parameters which is used to characterise standard airline speed procedures for climb, cruise, and descent.

Section 5, Global Aircraft Parameters, defines the set of global aircraft parameters that are valid for all, or a group of, aircraft.

Section 6, File Structure, describes the files in which the BADA aircraft parameters are maintained. Five types of files are identified:

- Synonym Files listing the supported aircraft types;
- Operations Performance Files (OPF) containing the performance parameters for a specific aircraft type;
- Airline Procedures Files (APF) containing speed procedure parameters for a specific aircraft type;
- Performance Table Files (PTF) containing summary performance tables of true air speed, climb/descent rates and fuel consumption at various flight levels for a specific aircraft type;

- Global Parameters File (GPF) containing parameters that are valid for all aircraft or a group of aircraft for instance all turboprops or all military a/c.

Section 7, Remote File Access to BADA, provides instructions on how to remotely access BADA files from the EEC computing facilities over the Internet.

Three appendices are also provided with this document. Appendix A presents a summary list of all files contained in BADA Revision 3.0. A listing of the tar file contents available for remote data access is given in Appendix B. Appendix C gives an overview of all available aircraft models.

## 1.4 Referenced Documents

- RD1** User Manual for the Base of Aircraft Data (BADA) Revision 2.6; EEC Note No. 23/97; September 1997.
- RD2** Aircraft Type Designators, ICAO Document 8643/25; January 1997.
- RD3** Aircraft Modelling Standards for Future ATC Systems; Eurocontrol Division E1 Document No. 872003, July 1987.
- RD4** Manual of the ICAO Standard Atmosphere; ICAO Document No. 7488, 2nd Edition, 1964.
- RD5** BADA Configuration Management Manual; Internal EEC Note 4/B2.3/1995; October 1995.
- RD6** Design and User Manual for BADA Excel Spreadsheets, Issue 1.1; EEC Note 16/96; August 1996.
- RD7** Memo on the Calculation of Energy Share Factor; EEC/FAS/BYR/95/50; 22 November 1995.
- RD8** Revision Summary Document for the Base of Aircraft Data (BADA) Revision 3.0; EEC Note 7/98; March 1998.
- RD9** Aircraft Performance Summary Tables for the Base of Aircraft Data (BADA) Revision 3.0; EEC Note 8/98; March 1998.
- RD10** Aircraft Type Designators, ICAO Document 8643/23; January 1994.

## 1.5 Glossary of Acronyms

<b>AGL</b>	Above Ground Level
<b>APF</b>	Airlines Procedures File
<b>APO</b>	Centre for Aircraft Performance and Operations
<b>ASCII</b>	American Standard Code for the Interchange of Information
<b>ATM</b>	Air Traffic Management
<b>BADA</b>	Base of Aircraft Data
<b>CAS</b>	Calibrated Airspeed
<b>CRCO</b>	Central Route Charges Office
<b>EEC</b>	Eurocontrol Experimental Centre
<b>ESF</b>	Energy Share Factor
<b>IAS</b>	Indicated Airspeed
<b>ICAO</b>	International Civil Aviation Organisation
<b>ISA</b>	International Standard Atmosphere
<b>MASS</b>	Multi-Aircraft Simplified Simulator
<b>MLW</b>	Maximum Landing Weight
<b>MTOW</b>	Maximum Take-off Weight
<b>OPF</b>	Operations Performance File
<b>OWE</b>	Operational Weight Empty
<b>PTF</b>	Performance Table File
<b>RCS</b>	Revision Control System
<b>ROCD</b>	Rate of Climb or Descent
<b>TAS</b>	True Airspeed
<b>TEM</b>	Total-Energy Model

## 1.6 Glossary of Symbols

A list of the symbols used in equations throughout this document is given below along with a description. Where appropriate, the engineering units typically associated with the symbol is also given.

a	speed of sound	[m/s]
d	distance	[ nautical miles ]
f	fuel flow	[ kg/min ]
g	gravitational acceleration	[m/s <sup>2</sup> ]
$\frac{dh}{dt}$	rate of climb or descent	[m/s] or [ft/min]
h	altitude above sea level	[metres] or [ft]
C	general coefficient	
D	drag force	[ Newtons ]
m	aircraft mass	[tonnes] or [ kg ]
M	Mach number	
R	real gas constant for air	[ m <sup>2</sup> /Ks <sup>2</sup> ]
S	reference wing surface area	[ m <sup>2</sup> ]
T	thrust temperature	[ N ] [ Kelvin ]
V	speed	[m/s] or [knots]
$\Delta T$	temperature difference	[ Kelvin ]
$\eta$	thrust specific fuel flow	[ kg / min / kN ]
$\rho$	air density	[ kg / m <sup>3</sup> ]

## 2. REVISION SUMMARY

This section summarises the aircraft types that are supported in BADA Revision 3.0 along with the updates that have been made from the previous release, BADA Revision 2.6.

### 2.1 Supported Aircraft

BADA 3.0 provides operations and procedures data for a total of 151 aircraft types. For 67 of these aircraft types, data is provided directly in files. These aircraft types are referred to as being directly supported. For the other 84 aircraft types, the data is specified to be the same as one of the directly supported 67 aircraft types. This second set of aircraft types are referred to as being supported through equivalence.

With one exception, each supported aircraft type is identified by a 4-character designation code assigned by the International Civil Aviation Organisation (ICAO) [RD2]. The exception is the model representing a generic military fighter which uses the designator: FGTR. Note that BADA 3.0 is the first release to use the new standard [RD2] which has had a significant impact (see Section 2.2).

The list of aircraft types supported by BADA 3.0 is given in Appendix C. In this Appendix the supported aircraft types are listed alphabetically by their designation code. For each aircraft type the aircraft name and type of BADA support (either direct or equivalence) is specified. Also, for each aircraft which is supported through equivalence, the corresponding equivalent aircraft type is specified.

### 2.2 Updates for BADA Revision 3.0

Updates made to BADA Revision 3.0 from the previous revision 2.6 are listed below:

- (a) Climb speed law changed for jet aircraft (Section 4.1 )
- (b) Descent speed law changed for jet, turbo and piston (Section 4.3 )
- (c) Reduced power climbs (Section 3.8 )
- (d) B777, SB20, B73X models were added
- (e) DA01 model removed
- (f) Use of the ICAO doc. 8643/25 standard. In certain cases this document combines several old designators to one new designator. This had led to the removal of 4 models. A number of equivalenced models were also removed.
- (g) B73F and B757 have been remodelled
- (h) MD90 added as an equivalent of the MD80
- (i) Cruise and descent speeds (.APF file) were changed for several turboprops
- (j) Climb thrust changed for several models

- (k) Expression for  $\rho_{\text{Trop}}$  added (Section 3.2 )
- (l) Extended description of the use of cruise thrust (Section 3.7.3 )
- (m) Removal of  $C_{m16}$  from drag expression (Section 3.6.1)

A more complete overview of all changes can be found in [RD8].

### 3. OPERATIONS PERFORMANCE MODEL

This section defines the various equations and coefficients used by the BADA operations performance model.

The first two subsections describe the Total-Energy Model (TEM) equations and standard atmosphere equations respectively.

The remaining eight subsections define the aircraft model in terms of the eight categories listed below.

- aircraft type,
- mass,
- flight envelope,
- aerodynamics,
- engine thrust,
- reduced power,
- fuel consumption and
- ground movement

#### 3.1 Total-Energy Model

The Total-Energy Model equates the rate of work done by forces acting on the aircraft to the rate of increase in potential and kinetic energy, that is:

$$(T - D)V_{TAS} = mg \frac{dh}{dt} + mV_{TAS} \frac{dV_{TAS}}{dt} \quad (3.1-1)$$

The symbols are defined below with metric units specified:

T	-	thrust acting parallel to the aircraft velocity vector	[Newtons]
D	-	aerodynamic drag	[Newtons]
m	-	aircraft mass	[kilograms]
h	-	altitude	[m]
g	-	gravitational acceleration	[9.81 m/s <sup>2</sup> ]
V <sub>TAS</sub>	-	true airspeed	[m/s]
$\frac{d}{dt}$	-	time derivative	[s <sup>-1</sup> ]

Note that true airspeed is often calculated in knots and altitude calculated in feet thus requiring the appropriate conversion factors.

Without considering the use of devices such as spoilers, leading-edge slats or trailing-edge flaps, there are two independent control inputs available for affecting the aircraft trajectory in the vertical plane. These are the throttle and the elevator.

These inputs allow any two of the three variables of thrust, speed, or ROCD to be controlled. The other variable is then determined by equation 3.1-1. The three resulting control possibilities are elaborated on below.

- (a) Speed and Throttle Controlled - Calculation of Rate of Climb or Descent

Assuming that velocity and thrust are independently controlled, then equation 3.1-1 is used to calculate the resulting rate of climb or descent (ROCD). This is a fairly common case for climbs and descents in which the throttle is set to some fixed position (maximum climb thrust or idle for descent) and the speed is maintained at some constant value of calibrated airspeed (CAS) or Mach number.

- (b) ROCD and Throttle Controlled - Calculation of Speed

Assuming that the ROCD and thrust are independently controlled, then equation 3.1-1 is used to calculate the resulting speed.

- (c) Speed and ROCD Controlled - Calculation of Thrust

Assuming that both ROCD and speed are controlled, then equation 3.1-1 can be used to calculate the necessary thrust. This thrust must be within the available limits for the desired ROCD and speed to be maintained.

Case (a), above, is the most common such that equation 3.1-1 is most often used to calculate the rate of climb or descent. To facilitate this calculation, equation 3.1-1 can be rearranged as follows:

$$(T - D)V_{TAS} = mg \frac{dh}{dt} + mV_{TAS} \left( \frac{dV_{TAS}}{dh} \right) \left( \frac{dh}{dt} \right) \quad (3.1-2)$$

Isolating the rate of climb or descent on the left hand side gives:

$$\frac{dh}{dt} = \frac{(T - D)V_{TAS}}{mg} \left[ 1 + \left( \frac{V_{TAS}}{g} \right) \left( \frac{dV_{TAS}}{dh} \right) \right]^{-1} \quad (3.1-3)$$

It has been shown by Renteux [RD3] that the last term can be replaced by an energy share factor as a function of Mach number,  $f\{M\}$ , as follows:

$$\frac{dh}{dt} = \left[ \frac{(T - D)V_{TAS}}{mg} \right] f\{M\} \quad (3.1-4)$$

This Energy Share Factor (ESF) specifies how much of the available power is allocated to climb as opposed to acceleration.

For several common flight conditions equation 3.1-4 can be rewritten as is done below. A more comprehensive description of this process can be found in RD7:

- (a) Constant Mach number in stratosphere (i.e. above tropopause)

$$f\{M\} = 1.0 \quad (3.1-5)$$

Note that above the tropopause (approximately 11000 metres under ISA conditions) the air temperature and the speed of sound is constant. Maintaining a constant Mach number therefore requires no acceleration and all available power can be allocated to a change in altitude.

- (b) Constant Mach number below tropopause:

$$f_{\text{share}} = \left[ 1 + \frac{\gamma R k_T}{2g} M^2 \right]^{-1} \quad (3.1-6)$$

where,

- R is the real gas constant for air,  $R = 287.04 \text{ m}^2/\text{Ks}^2$
- $g$  is the gravitational acceleration,  $g = 9.81 \text{ m/s}^2$
- $k_T$  is the ISA temperature gradient with altitude below the tropopause,  $k_T = -0.0065 \text{ K/m}$
- M is the Mach number, and,
- $\gamma$  is the isentropic expansion coefficient for air,  $\gamma = 1.4$

In this case, for a typical Mach number of 0.8 the energy share factor allocated to climb is 1.09.

This number is greater than 1 because below the tropopause, the temperature and thus speed of sound decreases with altitude. Maintaining a constant Mach number during climb thus means that the true air speed decreases with altitude. Thus, the rate of climb benefits from not only all the available power but also a transfer of kinetic energy to potential energy.

- (c) Constant Calibrated Airspeed (CAS) below tropopause

$$f_{\text{share}} = \left\{ 1 + \frac{\gamma R k_T}{2g} M^2 + \left( 1 + \frac{\gamma - 1}{2} M^2 \right)^{\frac{-1}{\gamma - 1}} \left\{ \left( 1 + \frac{\gamma - 1}{2} M^2 \right)^{\frac{\gamma}{\gamma - 1}} - 1 \right\} \right\}^{-1} \quad (3.1-7)$$

In this case the energy share factor is less than one. A Mach number of 0.6 for example yields an energy share factor of 0.85.

This number is less than 1 because as density decreases with altitude, maintaining a constant CAS during climb requires maintaining a continual increase in true air speed. Thus, some of the available power needs to be allocated to acceleration leaving the remainder for climb.

## (d) Constant Calibrated Airspeed (CAS) above tropopause

$$f_{\text{share}} = \left\{ 1 + \left( 1 + \frac{\gamma - 1}{2} M^2 \right)^{\frac{-1}{\gamma-1}} \left[ \left( 1 + \frac{\gamma - 1}{2} M^2 \right)^{\frac{\gamma}{\gamma-1}} - 1 \right] \right\}^{-1} \quad (3.1-8)$$

This is a very uncommon situation that would only occur at very low temperatures (ISA -20 or below) and it is therefore not incorporated in BADA, but merely mentioned for the sake of completeness.

The energy share factors given above apply equally well to descent as to climb. The difference being that the available power is negative for descent.

In cases where a constant Mach number or constant CAS is not maintained, the following energy share factors are specified by the BADA model.

acceleration in climb               $f\{M\} = 0.3$

deceleration in descent               $f\{M\} = 0.3$

deceleration in climb               $f\{M\} = 1.7$

acceleration in descent               $f\{M\} = 1.7$

Note for the cases of acceleration in climb or deceleration in descent, the majority of the available power is devoted to a change in speed.

For the cases of deceleration in climb or acceleration in descent, the energy share factor is greater than one since the change of altitude benefits from a transfer of kinetic energy.

### 3.2 Standard Atmosphere

Calculations for lift, drag, and conversions from CAS to TAS and Mach number require the determination of several atmospheric properties as a function of altitude.

The equations used by BADA for the standard atmosphere and CAS/TAS conversion are summarised below. These equations are based on the International Standard Atmosphere (ISA) [RD4].

(a) Determination of the Tropopause

$$h_{\text{trop}} = 11000 + 1000 \Delta T_{\text{ISA}} / 6.5 \quad (3.2-1)$$

Here the tropopause altitude,  $h_{\text{trop}}$ , is specified in metres.

$\Delta T_{\text{ISA}}$  is the temperature difference from the International Standard Atmosphere (ISA). That is, the temperature at sea level,  $T_0$ , would be:

$$T_0 = (T_0)_{\text{ISA}} + \Delta T_{\text{ISA}} \quad (3.2-2)$$

$$(T_0)_{\text{ISA}} = 288.15 \text{ K} \quad (3.2-3)$$

For standard atmosphere conditions, ( $\Delta T_{\text{ISA}} = 0$ ) the tropopause is at 11000 metres altitude.

(b) Determination of Temperature

Above the tropopause, the temperature is a constant, that is,

$$T_{\text{trop}} = 216.65 \text{ K} \quad (3.2-4)$$

Below the tropopause, the temperature is calculated as a function of altitude as follows:

$$T = T_0 - 6.5 * h / 1000 \quad (3.2-5)$$

Here the altitude,  $h$ , is specified in metres.

(c) Determination of Air Density

Below the tropopause, the air density,  $\rho$ , in  $\text{kg/m}^3$  is calculated as function of temperature as follows:

$$\rho = \rho_0 [T / T_0]^{4.255876} \quad (3.2-6)$$

Here  $\rho_0$  is the air density at sea level:

$$\rho_0 = (\rho_0)_{ISA} (T_0)_{ISA} / T_0 \quad (3.2-7)$$

and  $(\rho_0)_{ISA}$  is the standard atmosphere air density at sea level:

$$(\rho_0)_{ISA} = 1.225 \text{ kg/m}^3 \quad (3.2-8)$$

Above the tropopause, the air density,  $\rho$ , in  $\text{kg/m}^3$  is calculated as follows [RD4]:

$$\rho = \rho_{Trop} * e^{-\left(\frac{g}{R * T_{Trop}}\right) * (h - 11000)} \quad (3.2-9)$$

Here  $h$  represents the altitude in meters.

For the density at the tropopause ( $\rho_{Trop}$ ) the following expression can be used:

$$\rho_{Trop} = (\rho_0)_{ISA} (T_0)_{ISA} / T_{Trop} \quad (3.2-10)$$

#### (d) Determination of Sound Speed

Above the tropopause the speed of sound,  $a$ , is a constant:

$$a_{trop} = 295.07 \text{ m/s} \quad (3.2-11)$$

Below the tropopause, the speed of sound is calculated as a function of temperature:

$$a = 340.29 \sqrt{\frac{T}{(T_0)_{ISA}}} \quad (3.2-12)$$

#### (e) CAS/TAS Conversion

The true air speed,  $V_{TAS}$ , is calculated as a function of the calibrated air speed,  $V_{CAS}$ , as follows:

$$V_{TAS} = \left[ \frac{2 P}{\mu \rho} \left\{ \left( 1 + \frac{(\rho_0)_{ISA}}{P} \left[ \left( 1 + \frac{\mu}{2} \frac{(\rho_0)_{ISA}}{(\rho_0)_{ISA}} V_{CAS}^2 \right)^{1/\mu} - 1 \right]^\mu - 1 \right) \right\}^{1/2} \right] \quad (3.2-13)$$

Similarly,  $V_{CAS}$  is calculated as a function of  $V_{TAS}$  as follows:

$$V_{CAS} = \left[ \frac{2(P_0)_{ISA}}{\mu(\rho_0)_{ISA}} \left\{ \left( 1 + \frac{P}{(P_0)_{ISA}} \left[ \left( 1 + \frac{\mu \rho}{2 P} V_{TAS}^2 \right)^{1/\mu} - 1 \right] \right)^{\mu} - 1 \right\} \right]^{1/2} \quad (3.2-14)$$

where symbols not previously defined are explained below:

$$\mu = (\gamma - 1) / \gamma \quad (3.2-15)$$

$\gamma$  is the isentropic expansion coefficient for air = 1.4

P is the pressure at altitude [Pa]

$(P_0)_{ISA}$  is the ISA pressure at sea level = 101325 Pa

Also note that for these conversion formulas above, the speeds  $V_{TAS}$  and  $V_{CAS}$  must be specified in m/s.

The pressure at altitude, P, can be determined from the temperature at altitude, T, by the following formula which is valid for altitudes below the tropopause:

$$P = (P_0)_{ISA} \left( \frac{T}{T_0} \right)^{5.255876} \quad (3.2-16)$$

For altitudes above the tropopause, the following formula should be used:

$$P = P_{Trop} * e^{-\left( \frac{g}{R * T_{Trop}} \right) * (h - 11000)} \quad (3.2-17)$$

Where h is the altitude in meters.

#### (f) Mach/TAS conversion

$$V_{TAS} = M \sqrt{\gamma * R * T} \quad (3.2-18)$$

where,

- M is the Mach number,
- T is the local temperature at altitude,
- R is the universal gas constant for air = 287.04 [m<sup>2</sup>/Ks<sup>2</sup>], and,
- $\gamma$  is the isentropic expansion coefficient for air = 1.4

### 3.3 Aircraft Type

Three values are specified for aircraft type, these being the number of engines,  $n_{eng}$ , the engine type and the wake category.

The engine type can be one of three values:

- Jet,
- Turboprop, or,
- Piston.

The wake category can also be one of three values:

H	- heavy
M	- medium
L	- light

Note that the ICAO associates a wake category with each aircraft type designator [RD2].

### 3.4 Mass

Four mass values are specified for each aircraft in tonnes:

$m_{ref}$	- reference mass
$m_{min}$	- minimum mass
$m_{max}$	- maximum mass
$m_{pyld}$	- maximum payload mass

The reference mass is the mass for which other BADA performance coefficients are calculated.

Aircraft operating speeds vary with the aircraft mass. This variation is calculated according to the formula below:

$$V = V_{ref} \sqrt{\frac{m}{m_{ref}}} \quad (3.4-1)$$

In this formula, the aircraft reference speed  $V_{ref}$  is given for the reference mass  $m_{ref}$ . The speed at another mass,  $m$ , is then calculated as  $V$ .

An example of an aircraft speed which can be calculated via this formula is the stall speed,  $V_{stall}$ .

### 3.5 Flight Envelope

The maximum speed and altitude for the aircraft is expressed in terms of the following six parameters:

- $V_{MO}$  - maximum operating speed (CAS), in knots;
- $M_{MO}$  - maximum operational Mach number;
- $h_{MO}$  - maximum operational height, in feet above sea level;
- $h_{max}$  - maximum altitude (300 fpm) at MTOW under ISA conditions;
- $G_w$  - mass gradient on maximum altitude;
- $G_t$  - temperature gradient on maximum altitude;

where the maximum altitude for any given mass is:

$$h_{max/act} = \text{MIN}(h_{MO}, h_{max} + G_t * (\Delta T_{ISA} - C_{tc4}) + G_w * (m_{max} - m_{act})) \quad (3.5-1)$$

with:  $G_w \geq 0$ ;

$G_t \leq 0$ ;

if  $(\Delta T_{ISA} - C_{tc4}) < 0$ , then :  $(\Delta T_{ISA} - C_{tc4}) = 0$ ;

with  $\Delta T_{ISA}$  being the temperature deviation from ISA and  $m_{act}$  being the actual aircraft mass (kg). Formula 3.5-1 should not be executed when the  $h_{max}$  value in the .OPF file is set to 0 (zero). In that case the maximum altitude is always  $h_{MO}$ .

The minimum speed for the aircraft is specified as follows:

$$V_{min} = C_{Vmin, TO} * V_{stall} \quad \text{if in take-off} \quad (3.5-2)$$

$$V_{min} = C_{Vmin} * V_{stall} \quad \text{otherwise} \quad (3.5-3)$$

Note: See 3.6.2 for minimum speed at high altitude for jet aircraft and Section 5.7 for the values of the minimum speed coefficients.

Here the speeds are specified in terms of CAS. The stall speed depends upon the configuration. Specifically, five different configurations are specified with a stall speed given for each:

TO - take-off configuration  $(V_{stall})_{TO}$   
(up to 400 ft AGL)

IC - initial climb configuration  $(V_{stall})_{IC}$   
(between 400 and 3000 ft AGL)

CR - cruise (clean) configuration  $(V_{stall})_{CR}$   
 (above 2000 ft AGL in climb,  
 in descent above 8,000 ft and,  
 in descent below 8,000 ft as long as  $V > V_{min_{Cruise}} + 10 \text{ kts}$  )

AP - approach configuration  $(V_{stall})_{AP}$   
 (in descent below 8,000 ft when  $V < V_{min_{Cruise}} + 10 \text{ kts}$  )

LD - landing configuration  $(V_{stall})_{LD}$   
 (in descent below 3,000 ft when  $V < V_{min_{Approach}} + 10 \text{ kts}$  )

Note that these stall speeds correspond to a minimum stall speed and not a 1-g stall speed. Also, the BADA model assumes that for any aircraft these stall speeds have the following relationship:

$$(V_{stall})_{CR} \geq (V_{stall})_{IC} \geq (V_{stall})_{TO} \geq (V_{stall})_{AP} \geq (V_{stall})_{LD}$$

## 3.6 Aerodynamics

### 3.6.1 Aerodynamic Drag

Under nominal conditions, the drag coefficient,  $C_D$  is specified as a function of the lift coefficient  $C_L$  as follows:

$$C_D = (C_{D0,CR} + C_{D2,CR} C_L^2) \quad (3.6-1)$$

Formula 3.6-1 is valid for all situation except for the approach and landing where other drag coefficients are to be used.

In the approach phase a different flap setting is used. Formula 3.6-2 should be applied below 10,000 ft when the aircraft descends and the speed falls below  $V_{min,Cruise} + 10$  kts for the clean configuration (corrected for aircraft mass). Note that  $V_{min,Cruise} = 1.3 * V_{stall,Cruise}$ .

$$C_D = (C_{D0,AP} + C_{D2,AP} C_L^2) \quad (3.6-2)$$

In the landing phase Formula 3.6-3 is used. This formula is applied below 10,000 ft when the aircraft descends and as soon as the speed falls below  $V_{min,Approach} + 10$  kts, where  $V_{min,Approach} = 1.3 * V_{stall,Approach}$ .

$$C_D = (C_{D0,LD} + C_{D0,ALDG} + C_{D2,LD} C_L^2) \quad (3.6-3)$$

The value of  $C_{D0,ALDG}$  is a function of the flap setting. The values of  $C_{D0,ALDG}$  in the <A/C>\_\_.OPF files were all determined for the landing flap setting mentioned in the OPF file. The drag force in Newtons is then determined from the drag coefficient in the standard manner:

$$D = C_D * \rho * V_{TAS}^2 * S / 2 \quad (3.6-4)$$

where  $\rho$  is the air density ( $\text{kg/m}^3$ ),  $S$  is the wing reference area ( $\text{m}^2$ ), and  $V_{TAS}$  is the true airspeed (m/s). Note that the air density is a function of altitude as described in subsection 3.2.

The lift coefficient,  $C_L$ , is determined assuming that the flight path angle is zero, however a correction for bank angle is made:

$$C_L = 2 * m * g / \rho * V_{TAS}^2 * S * \cos(\phi) \quad (3.6-5)$$

The above equations thus result in nine coefficients for the specification of drag:  $S$ ,  $C_{D0,CR}$ ,  $C_{D2,CR}$ ,  $C_{D0,AP}$ ,  $C_{D2,AP}$ ,  $C_{D0,LD}$ ,  $C_{D2,LD}$ ,  $C_{D0,ALDG}$  and  $C_{M16}$ . In case the  $C_{D0,AP}$ ,  $C_{D2,AP}$ ,  $C_{D0,LD}$ ,  $C_{D2,LD}$  and  $C_{D0,ALDG}$  coefficients are set to 0 (zero) in the OPF file, expression 3.6-1 will be used in all cases.

### 3.6.2 Low Speed Buffeting Limit (jet aircraft only)

For jet aircraft a low speed buffeting limit has been introduced. This buffeting limit is expressed as a Mach number and can be determined using the following equation:

$$k*M^3 - C_{Lbo(M=0)}*M^2 + (W/S) / (0.583*P) = 0 \quad (3.6-6)$$

Note that the factor of 0.583 gives a 0.2g margin. The W, S and P parameters are already known in BADA. The k and  $C_{Lbo(M=0)}$  parameters have been determined for nearly all jet aircraft in BADA 3.0. The solution for M in Formula 3.6-4 can be obtained using the method given in Appendix D of RD1. The buffeting limit should be applied as a minimum speed in the following way:

If (Altitude > 15,000 ft) then:  $V_{min} = MAX(1.3*V_{stall}, M_b)$

If (Altitude < 15,000 ft) then:  $V_{min} =$  expressions 3.5-2, 3.5-3

where  $M_b$  is the lowest positive solution of expression 3.6-4. Note that the units of the two values inside the MAX() expression should be the same.

If the k and  $C_{Lbo(M=0)}$  parameters in the OPF file are set to 0 (zero), the minimum speed above 15,000 ft is  $1.3*V_{stall}$ .

## 3.7 Engine Thrust

The BADA model provides coefficients that allow the calculation of the following thrust levels:

- maximum climb,
- nominal climb
- maximum take-off,
- maximum cruise, and,
- descent

The thrust is calculated in Newtons and includes the contribution from all engines. The subsections below provide the equations for each of the four thrust conditions.

### 3.7.1 Maximum Climb Thrust

The maximum climb thrust at standard atmosphere conditions,  $(T_{\max \text{ climb}})_{\text{ISA}}$ , is calculated in Newtons as a function of the following:

- engine type: either Jet, Turboprop or Piston;
- altitude above sea level,  $h$ , in feet;
- true air speed,  $V_{\text{TAS}}$ , in knots; and,
- temperature deviation from standard atmosphere,  $\Delta T_{\text{ISA}}$ , in degrees Celsius.

The equations corresponding to the three engine types are given below.

$$\text{Jet: } (T_{\max \text{ climb}})_{\text{ISA}} = C_{Tc,1} (1 - h/C_{Tc,2} + C_{Tc,3} h^2) \quad (3.7-1)$$

$$\text{Turboprop: } (T_{\max \text{ climb}})_{\text{ISA}} = C_{Tc,1} (1 - h/C_{Tc,2})/V_{\text{TAS}} + C_{Tc,3} \quad (3.7-2)$$

$$\text{Piston: } (T_{\max \text{ climb}})_{\text{ISA}} = C_{Tc,1} (1 - h/C_{Tc,2}) + C_{Tc,3}/V_{\text{TAS}} \quad (3.7-3)$$

For all engine types, the maximum climb thrust is corrected for temperature deviations from standard atmosphere,  $\Delta T_{\text{ISA}}$ , in the following manner:

$$T_{\max \text{ climb}} = (T_{\max \text{ climb}})_{\text{ISA}} [1 - C_{Tc,5}(\Delta T_{\text{ISA}})_{\text{eff}}] \quad (3.7-4)$$

$$\text{where } (\Delta T_{\text{ISA}})_{\text{eff}} = \Delta T_{\text{ISA}} - C_{Tc,4} \quad (3.7-5)$$

$$\text{with the limit: } 0.0 \leq (\Delta T_{\text{ISA}})_{\text{eff}} * C_{Tc,5} \leq 0.4 \quad (3.7-6)$$

$$\text{and: } C_{Tc,5} \geq 0.0 \quad (3.7-7)$$

### 3.7.2 Maximum Take-Off Thrust

The maximum take-off thrust is specified to be a ratio of the maximum climb thrust, that is:

$$(T_{\text{take-off}})_{\text{max}} = C_{\text{Tto}} * T_{\text{max climb}} \quad (3.7-8)$$

This factor of  $C_{\text{Tto}}$  is applied at flight levels below 400 ft and is the same for all aircraft and all aircraft types (jet, turboprop or piston). The current value is 1.2.

### 3.7.3 Maximum Cruise Thrust

The normal cruise thrust is by definition set equal to drag ( $T = D$ ). However the amount of thrust that is available in cruise situations is limited. The maximum cruise thrust is calculated as a ratio of the maximum climb thrust given in section 3.7.1, that is:

$$(T_{\text{cruise}})_{\text{max}} = C_{\text{Tcr}} * T_{\text{max climb}} \quad (3.7-9)$$

The coefficient  $C_{\text{Tcr}}$  is currently uniformly set to 0.95 for all aircraft.

### 3.7.4 Descent Thrust

Descent thrust is calculated similarly to cruise thrust with different correction factors used for high and low altitude and approach and landing configurations, that is:

if  $h > h_{\text{des}}$

$$T_{\text{des,high}} = C_{\text{Tdes,high}} * T_{\text{max climb}} \quad (3.7-10)$$

if  $h < h_{\text{des}}$

$$T_{\text{des,low}} = C_{\text{Tdes,low}} * T_{\text{max climb}} \quad (3.7-11)$$

Once the aircraft has descended below 8,000 ft it changes configuration as soon as the airspeed falls below a certain threshold (Section 3.5). At the same time the thrust setting is changed as well as detailed below:

if  $h < 8,000$  ft and  $V < V_{\text{min,Cruise}} + 10$  kts

$$T_{\text{des,app}} = C_{\text{Tdes,app}} * T_{\text{max climb}} \quad (3.7-12)$$

if  $h < 3,000$  ft and  $V < V_{\text{min,Approach}} + 10$  kts

$$T_{\text{des,ld}} = C_{\text{Tdes,ld}} * T_{\text{max climb}} \quad (3.7-13)$$

In case the  $C_{\text{Tdes,app}}$  and  $C_{\text{Tdes,ld}}$  are set to 0 (zero) in the OPF file, expression 3.7-11 must be used in all cases where  $h < h_{\text{des}}$ . For those models where non-clean data is available,  $h_{\text{des}}$  cannot be below 8,000 ft. Note that the speeds (V) used during the descent, approach and landing phase are defined in Section 4.3.

### 3.8 Reduced Climb Power

The reduced climb power has been introduced to allow the simulation of climbs using less than the maximum climb setting. In day-to-day operations, many aircraft use a reduced setting during climb in order to extend engine life and save cost. The correction factors that are used to calculate the reduction in power have been obtained in an empirical way and have been validated with the help of air traffic controllers.

In BADA, climbs that are performed using the full climb power will result in profiles that match the reference data that is found in the Flight Manual of the aircraft. Climbs with reduced power will give a realistic profile.

$$C_{\text{pow,red}} = 1 - C_{\text{red}} * \{(m_{\text{max}} - m_{\text{act}}) / (m_{\text{max}} - m_{\text{min}})\} \quad (3.8-1)$$

The value of  $C_{\text{red}}$  is a function of the aircraft type and is given in the BADA.GPF file (see Section 5.11).

$C_{\text{pow,red}}$  is to be used in the following expression:

$$P = (T_{\text{max,climb}} - D) * V * C_{\text{pow,red}} \quad (3.8-2)$$

The power reduction is to be applied in the Initial Climb and Climb phases.

### 3.9 Fuel Consumption

The thrust specific fuel consumption,  $\eta$ , in kg/minute/kN is specified as a function of true airspeed,  $V_{TAS}$  (knots) for the jet and turboprop engines. The nominal fuel flow,  $f_{nom}$  (kg/minute), can then be calculated using the thrust, T:

$$\text{jet: } \eta = C_{f1} (1 + V_{TAS} / C_{f2}) \quad (3.9-1)$$

with:

$$f_{nom} = \eta * T \quad (3.9-2)$$

$$\text{turboprop: } \eta = C_{f1} (1 - V_{TAS} / C_{f2})(V_{TAS} / 1000) \quad (3.9-3)$$

with:

$$f_{nom} = \eta * T \quad (3.9-4)$$

These expressions are used in all flight phases except during cruise and for descent/idle conditions.

Minimum fuel flow,  $f_{min}$ , corresponding to idle thrust or descent conditions for both jets and turboprop engines is specified in kg/minute as a function of altitude above sea level, h (ft), that is:

$$\text{jet/turboprop: } f_{min} = C_{f3} (1 - h / C_{f4}) \quad (3.9-5)$$

Cruise fuel flow,  $f_{cr}$ , is calculated using the thrust specific fuel consumption and a cruise fuel flow factor:

$$\text{jet/turboprop: } f_{cr} = \eta * T * C_{fcf} \quad (3.9-6)$$

For piston engines the fuel flow,  $f$ , in kg/minutes is specified to be a constant, that is,

$$\text{piston: } f_{cr} = C_{f1} * C_{fcf} \quad (\text{cruise}) \quad (3.9-7)$$

$$f_{min} = C_{f3} \quad (\text{idle/descent}) \quad (3.9-8)$$

$$f_{nom} = C_{f1} \quad (\text{all other phases}) \quad (3.9-9)$$

For the moment the cruise fuel flow correction factor has been established for a number of aircraft. This factor has been set to 1 (one) for all the other aircraft models.

### 3.10 Ground Movement

Four values are specified that can be of use when simulating ground movements. These parameters are:

- TOL: - FAR Take-Off Length with MTOW on a dry, hard, level runway under ISA conditions and no wind [m].
- LDL: - FAR Landing Length with MLW on a dry, hard, level runway under ISA conditions and no wind [m].
- span: - Aircraft wingspan [m]
- length: - Aircraft length [m]

Note that currently the value of the MLW is not defined in BADA. Apart from these model specific parameters, there are also a number of groundspeeds defined as general parameters in the BADA.GPF file, see Section 5.10.

### 3.11 Summary of Operations Performance Parameters

A summary of the parameters specified by the BADA operations performance model is supplied in Table 3.11-1 below. This table excludes those parameters that have been set to zero.

**Table 3.11-1: BADA Operations Performance Parameter Summary**

Model Category	Symbols	Units	Description
aircraft type (3 values)	$n_{eng}$ engine type wake category	dimensionless string string	number of engines either Jet, Turboprop or Piston either H (heavy), M (medium) or L (light)
mass (4 values)	$m_{ref}$ $m_{min}$ $m_{max}$ $m_{pyld}$	tonnes tonnes tonnes tonnes	reference mass minimum mass maximum mass maximum payload mass
flight envelope (6 values)	$V_{MO}$ $M_{MO}$ $h_{MO}$ $h_{max}$ $G_w$ $G_t$	knots (CAS) dimensionless feet feet feet/kg feet/C	maximum operating speed maximum operating Mach number maximum operating altitude maximum altitude at MTOW and ISA weight gradient on maximum altitude temperature gradient on maximum altitude
Aerodynamics (14 values) (16 values for jet aircraft)	$S$ $C_{D0\ CR}$ $C_{D2\ CR}$ $C_{D0\ AP}$ $C_{D2\ AP}$ $C_{D0\ LD}$ $C_{D2\ LD}$ $C_{D0\ ALDG}$  $C_{M16}$ $(V_{stall})_1$  $C_{Lbo(M=0)}$ $k$	$m^2$ dimensionless dimensionless dimensionless dimensionless dimensionless dimensionless dimensionless  dimensionless knots (CAS)  dimensionless [1/M]	reference wing surface area parasitic drag coefficient (cruise) induced drag coefficient (cruise) parasitic drag coefficient (approach) induced drag coefficient (approach) parasitic drag coefficient (landing) induced drag coefficient (landing) parasite drag coefficient (landing gear)  Mach drag coefficient stall speed for various configuration [TO, IC, CR, AP, LD]  Buffet onset lift coefficient (jet only) Buffeting gradient (jet only)

**Table 3.11-1: BADA Operations Performance Parameter Summary (continued)**

Model Category	Symbols	Units	Description
engine thrust (12 values)	$C_{Tc,1}$	Newton (jet/piston) knot-Newton (turboprop)	1 <sup>st</sup> max. climb thrust coefficient
	$C_{Tc,2}$	feet	2 <sup>nd</sup> max climb thrust coefficient
	$C_{Tc,3}$	1/feet <sup>2</sup> (jet) Newton (turboprop) knot-Newton (piston)	3 <sup>rd</sup> max. climb thrust coefficient
	$C_{Tc,4}$	deg. C	1 <sup>st</sup> thrust temperature coefficient
	$C_{Tc,5}$	1/ deg. C	2 <sup>nd</sup> thrust temperature coefficient
	$C_{Tdes,low}$	dimensionless	low altitude descent thrust coefficient
	$C_{Tdes,high}$	dimensionless	high altitude descent thrust coefficient
	$h_{des}$	feet	transition altitude for calculation of descent thrust
	$C_{Tdes,app}$	dimensionless	approach thrust coefficient
	$C_{Tdes,ld}$	dimensionless	landing thrust coefficient
fuel flow (5 values)	$V_{des,ref}$	knots	reference descent speed (CAS)
	$M_{des,ref}$	dimensionless	reference descent Mach number
	$C_{f1}$	kg/min/kN (jet) kg/min/kN/knot (turboprop) kg/min (piston)	1 <sup>st</sup> thrust specific fuel consumption coefficient
	$C_{f2}$	knots	2 <sup>nd</sup> thrust specific fuel consumption coefficient
	$C_{f3}$	kg/min	1st descent fuel flow coefficient
	$C_{f4}$	feet	2nd descent fuel flow coefficient
	$C_{fer}$	dimensionless	Cruise fuel flow correction coefficient

**Table 3.11-1: BADA Operations Performance Parameter Summary (continued)**

ground movement (4 values)	TOL	m	take-off length
	LDL	m	landing length
	span	m	wingspan
	length	m	length

The total number of BADA performance coefficients summarised in the above table is 51.

## 4. AIRLINE PROCEDURE MODELS

This section defines the standard airline procedures which are parameterised by the BADA procedures model. Three separate flight phases are considered:

- climb,
- cruise, and,
- descent.

Each of these phases is described in the subsections below. Note that  $C_{V_{\min}}$  in the sections below always has the value of 1.3 unless the aircraft is in the take-off phase (below 400 ft) in which case the value is 1.2 (see also Section 5.7).

### 4.1 Climb

The following parameters are defined for each aircraft type to characterise the climb phase:

$V_{cl,1}$	-	standard climb CAS (knots) between 1,500 / 6,000 and 10,000 ft
$V_{cl,2}$	-	standard climb CAS (knots) between 10,000 ft and Mach transition altitude
$M_{cl}$	-	standard climb Mach number above transition altitude

Note that the Mach transition altitude is defined to be the altitude where a CAS value corresponding to  $V_{cl,2}$  results in a Mach number of  $M_{cl}$ . That is,  $M_{cl}$  imposes an upper limit on the Mach number during climb.

For jet aircraft the following CAS schedule is assumed, based on the parameters mentioned above and the take-off stall speed:

$$\text{from 0 to 1,499 ft} \quad C_{V_{\min}} * (V_{stall})_{TO} + Vd_{CL,1} \quad (4.1-1)$$

$$\text{from 1,500 to 2,999 ft} \quad C_{V_{\min}} * (V_{stall})_{TO} + Vd_{CL,2} \quad (4.1-2)$$

$$\text{from 3,000 to 3,999 ft} \quad C_{V_{\min}} * (V_{stall})_{TO} + Vd_{CL,3} \quad (4.1-3)$$

$$\text{from 4,000 to 4,999 ft} \quad C_{V_{\min}} * (V_{stall})_{TO} + Vd_{CL,4} \quad (4.1-4)$$

$$\text{from 5,000 to 5,999 ft} \quad C_{V_{\min}} * (V_{stall})_{TO} + Vd_{CL,5} \quad (4.1-5)$$

$$\text{from 6,000 to 9,999 ft} \quad V_{cl,1}$$

$$\text{from 10,000 ft to transition} \quad V_{cl,2}$$

$$\text{above transition} \quad M_{cl}$$

Note : below 10,000 ft the CAS should be limited to 250 or  $V_{cl,1}$ , whichever is lower.

For turboprop and piston aircraft the following CAS schedule is assumed:

$$\text{from 0 to 499 ft} \quad C_{V_{\min}} * (V_{\text{stall}})_{\text{TO}} + Vd_{\text{CL}, 6} \quad (4.1-6)$$

$$\text{from 500 to 999 ft} \quad C_{V_{\min}} * (V_{\text{stall}})_{\text{TO}} + Vd_{\text{CL}, 7} \quad (4.1-7)$$

$$\text{from 1,000 to 1,499 ft} \quad C_{V_{\min}} * (V_{\text{stall}})_{\text{TO}} + Vd_{\text{CL}, 8} \quad (4.1-8)$$

$$\text{from 1,500 to 9,999 ft} \quad V_{\text{cl}, 1} \quad (\text{or 250 knots whichever is lower})$$

$$\text{from 10,000 ft to transition} \quad V_{\text{cl}, 2}$$

$$\text{above transition} \quad M_{\text{cl}}$$

Note : below 10,000 ft the CAS should be limited to 250 or  $V_{\text{cl}, 1}$ , whichever is lower

The take-off stall speed,  $(V_{\text{stall}})_{\text{TO}}$ , must be corrected for the difference in aircraft mass from the reference mass using the formula as described in Section 3.4. The values for  $Vd_{\text{CL}}$  can be found in Section 5.

Also, the transition altitude,  $h_{\text{trans}}$ , in feet for a given  $V_{\text{CAS}}$  (in m/s), and Mach number,  $M$ , can be calculated as follows:

$$h_{\text{trans}} = \left( \frac{1000}{(.3048)(6.5)} \right) [T_0(1 - \theta_{\text{trans}})] \quad (4.1-9)$$

where,

$T_0$  is the temperature at sea level in Kelvin,

$(T_0)_{\text{ISA}}$  is the ISA temperature at sea level = 288.15 K,

$\theta_{\text{trans}}$  is the temperature ratio at the transition altitude,

$$\theta_{\text{trans}} = (\delta_{\text{trans}})^{0.1903} \quad (4.1-10)$$

$\delta_{\text{trans}}$  is the pressure ratio at the transition altitude,

$$\delta_{\text{trans}} = \frac{\left[ 1 + \left( \frac{\gamma - 1}{2} \right) \left( \frac{V_{\text{CAS}}}{(a_0)_{\text{ISA}}} \right)^2 \right]^{\frac{\gamma}{\gamma-1}} - 1}{\left[ 1 + \frac{\gamma - 1}{2} M^2 \right]^{\frac{\gamma}{\gamma-1}} - 1} \quad (4.1-11)$$

$(a_0)_{\text{ISA}}$  is the ISA speed of sound at sea level = 340.29 m/s

## 4.2 Cruise

The following parameters are defined for each aircraft type to characterise the cruise phase:

- $V_{cr,1}$  - standard cruise CAS (knots) between 3,000 and 10,000 feet
- $V_{cr,2}$  - standard cruise CAS (knots) above 10,000 ft until Mach transition altitude
- $M_{cr}$  - standard cruise Mach number above transition altitude

From 3000 ft to 10000 ft, any aircraft is assumed to cruise with a constant CAS equal to  $V_{cr,1}$  or 250 knots whichever is lower.

Above 10000 ft, the cruise speed is assumed to be a constant CAS equal to  $V_{cl,2}$  until the transition altitude is reached. Above the transition altitude the aircraft is assumed to cruise with a constant Mach number equal to  $M_{cl}$ .

## 4.3 Descent

The following parameters are defined for each aircraft type to characterise the descent phase:

- $V_{des,1}$  - standard descent CAS (knots) between 1,500 / 6,000 and 10,000 ft
- $V_{des,2}$  - standard descent CAS (knots) above 10,000 ft until Mach transition
- $M_{des}$  - standard descent Mach number above transition altitude

For jet and turboprop aircraft the following CAS schedule is assumed, based on the above parameters and the landing stall speed:

$$\text{from 0 to } 999 \text{ ft} \quad C_{V_{min}} * (V_{stall})_{LD} + Vd_{DES,1} \quad (4.3-1)$$

$$\text{from 1,000 to } 1,499 \text{ ft} \quad C_{V_{min}} * (V_{stall})_{LD} + Vd_{DES,2} \quad (4.3-2)$$

$$\text{from 1,500 to } 1,999 \text{ ft} \quad C_{V_{min}} * (V_{stall})_{LD} + Vd_{DES,3} \quad (4.3-3)$$

$$\text{from 2,000 to } 2,999 \text{ ft} \quad C_{V_{min}} * (V_{stall})_{LD} + Vd_{DES,4} \quad (4.3-4)$$

$$\text{from 3,000 to } 5,999 \text{ ft} \quad \text{MIN} (V_{des,1}, 220) \quad (4.3-5)$$

$$\text{from 6,000 to } 9,999 \text{ ft} \quad \text{MIN} (V_{des,1}, 250) \quad (4.3-6)$$

$$\text{above } 10,000 \text{ ft to transition} \quad V_{des,2}$$

$$\text{above transition} \quad M_{des}$$

For piston aircraft the following CAS schedule is assumed:

$$\text{from 0 to 499 ft} \quad C_{V_{\min}} * (V_{\text{stall}})_{LD} + Vd_{DES,7} \quad (4.3-7)$$

$$\text{from 500 to 999 ft} \quad C_{V_{\min}} * (V_{\text{stall}})_{LD} + Vd_{DES,8} \quad (4.3-8)$$

$$\text{from 1000 to 1,499 ft} \quad C_{V_{\min}} * (V_{\text{stall}})_{LD} + Vd_{DES,9} \quad (4.3-9)$$

$$\text{above 1,500 ft to 9,999 ft} \quad V_{des,1}$$

$$\text{above 10,000 ft to transition} \quad V_{des,2}$$

$$\text{above transition} \quad M_{des}$$

The landing stall speed,  $(V_{\text{stall}})_{LD}$ , must be corrected for the difference in aircraft mass from the reference mass using formula 3.4-1. The values for  $Vd_{DES}$ , can be found in Section 5.

## 5 GLOBAL AIRCRAFT PARAMETERS

### 5.1 Introduction

A number of parameters that have been described in Section 3 (Operations Performance Model) and Section 4 (Airline Procedure Model) have values that are independent of the aircraft type or model for which they are used. The values of these and other parameters that up to BADA 2.4 were hard-coded in the aircraft navigator (MASS at the EEC), have been put in the General Parameters File (BADA.GPF). This increases the flexibility and allows an easier evaluation of the values that are used.

The next section gives an overview of the parameters that are defined in the Global Parameters File. If relevant, it also indicates the formula in which the parameter should be used.

### 5.2 Maximum Acceleration

Maximum acceleration parameters are used to limit the increment in TAS (longitudinal) or ROCD (normal). 2 parameters are defined:

Name:	Description:	Value [fps <sup>2</sup> ]:
$a_{l, \text{max (civ)}}$	maximum longitudinal acceleration for civil flights	2.0
$a_{n, \text{max (civ)}}$	maximum normal acceleration for civil flights	5.0

The two acceleration limits are to be used in the following way:

$$\text{longitudinal acceleration: } |V_k - V_{k-1}| \leq a_{l, \text{max (civ)}} \Delta t \quad (5.2-1)$$

$$\text{normal acceleration: } |\gamma_k - \gamma_{k-1}| \leq \frac{a_{n, \text{max (civ)}} \Delta t}{V} \quad (5.2-2)$$

where,

$$\gamma = \sin^{-1} \left( \frac{\dot{h}}{V} \right) \quad (5.2-3)$$

and,

- |            |  |
|------------|--|
| $\gamma$   | is the climb/descent angle,                          |
| $V$        | is the True Air Speed,                               |
| $k, k-1$   | indicates values at update intervals k and k-1, and, |
| $\Delta t$ | is the time interval between k and k-1               |

The values for  $a_{l, \text{max (mil)}}$  (maximum longitudinal acceleration for military flights ) and  $a_{n, \text{max (mil)}}$  (maximum normal acceleration for military flights ) are currently undefined.

### 5.3 Bank Angles

Nominal and maximum bank angles are defined separately for military and civil flights. These bank angles can be used to calculate nominal and maximum rate of turns.

<b>Name:</b>	<b>Description:</b>	<b>Value [degr.]:</b>
$\phi_{\text{nom, civ (TO, LD)}}$	Nominal bank angles for civil flight during TO and LD	15
$\phi_{\text{nom, civ (OTHERS)}}$	Nominal bank angles for civil flight during all other phases	35
$\phi_{\text{nom, mil}}$	Nominal bank angles for military flight (all phases)	50
$\phi_{\text{max, civ (TO, LD)}}$	Maximum bank angles for civil flight during TO and LD	25
$\phi_{\text{max, civ (HOLD)}}$	Maximum bank angles for civil flight during HOLD	30
$\phi_{\text{max, civ (OTHERS)}}$	Maximum bank angles for civil flight during all other phases	45
$\phi_{\text{max, mil}}$	Maximum bank angles for military flight (all phases)	70

The rate of turn ( $\dot{\phi}$ ) is calculated as a function of bank angle:  $\dot{\phi} = (g / V_{\text{TAS}}) * \tan(\phi)$  (5.3-1)

### 5.4 Expedited Descent

The expedited descent factor is to be used as a drag increment during expedited descents:

<b>Name:</b>	<b>Description:</b>	<b>Value [ - ]:</b>
$C_{\text{des, exp}}$	Expedited descent factor	1.6

The drag during an expedited descent is calculated using the nominal drag (see 3.6-2):

$$D_{\text{des, exp}} = C_{\text{des, exp}} * D_{\text{nom}} \quad (5.4-1)$$

### 5.5 Thrust Factors

Maximum take-off and maximum cruise thrust factors have been specified. These factors are to be used in expressions 3.7-8 and 3.7-9, respectively:

<b>Name:</b>	<b>Description:</b>	<b>Value [ - ]:</b>
$C_{\text{Th, to}}$	Take-off thrust coefficient	1.2
$C_{\text{Th, cr}}$	Maximum cruise thrust coefficient	0.95

### 5.6 Configuration Altitude Threshold

For 4 configurations, altitude thresholds have been specified in BADA: take-off (TO) and initial climb (IC). Note that the selection of the approach and landing configurations is done through the use of air speed (see Section 3.5) but the altitudes at which this takes place should not be higher than the ones mentioned below.

<b>Name:</b>	<b>Description:</b>	<b>Value [ ft ]:</b>
$H_{\max, \text{TO}}$	Maximum altitude threshold for take-off	400
$H_{\max, \text{IC}}$	Maximum altitude threshold for initial climb	2,000
$H_{\max, \text{AP}}$	Maximum altitude threshold for approach	8,000
$H_{\max, \text{LD}}$	Maximum altitude threshold for landing	3,000

## 5.7 Minimum Speed Coefficients

Two minimum speed coefficients are specified, which are to be used in expressions 3.5-2 and 3.5-3 and in Section 4.1, 4.2 and 4.3:

<b>Name:</b>	<b>Description:</b>	<b>Value [ - ]:</b>
$C_{V_{\min}, \text{TO}}$	Minimum speed coefficient for take-off	1.2
$C_{V_{\min}}$	Minimum speed coefficient (all other phases)	1.3

## 5.8 Speed Schedules

The speed schedules for climb and descent are based on a factored stall speed plus increment valid for a specified altitude range:

<b>Name:</b>	<b>Description:</b>	<b>Value[KCAS]:</b>
$Vd_{CL, 1}$	Climb speed increment below 1500 ft (jet)	5
$Vd_{CL, 2}$	Climb speed increment below 3000 ft (jet)	10
$Vd_{CL, 3}$	Climb speed increment below 4000 ft (jet)	30
$Vd_{CL, 4}$	Climb speed increment below 5000 ft (jet)	60
$Vd_{CL, 5}$	Climb speed increment below 6000 ft (jet)	80
$Vd_{CL, 6}$	Climb speed increment below 500 ft (turbo/piston)	20
$Vd_{CL, 7}$	Climb speed increment below 1000 ft (turbo/piston)	30
$Vd_{CL, 8}$	Climb speed increment below 1500 ft (turbo/piston)	35
$Vd_{DES, 1}$	Descent speed increment below 1000 ft (jet/turboprop)	5
$Vd_{DES, 2}$	Descent speed increment below 1500 ft (jet/turboprop)	10
$Vd_{DES, 3}$	Descent speed increment below 2000 ft (jet/turboprop)	20
$Vd_{DES, 4}$	Descent speed increment below 3000 ft (jet/turboprop)	50
$Vd_{DES, 5}$	Descent speed increment below 500 ft (piston)	5
$Vd_{DES, 6}$	Descent speed increment below 1000 ft (piston)	10
$Vd_{DES, 7}$	Descent speed increment below 1500 ft (piston)	20

These values are to be used in the expressions in Section 4.1, 4.2 and 4.3

## 5.9 Holding Speeds

The holding speeds that are to be used to calculate holding areas are defined according to the ICAO standards:

<b>Name:</b>	<b>Description:</b>	<b>Value[KCAS]:</b>
$V_{hold,1}$	Holding speed below FL140	230
$V_{hold,2}$	Holding speed between FL140 and FL200	240
$V_{hold,3}$	Holding speed between FL200 and FL340	265
$V_{hold,4}$	Holding speed above FL340	0.83 [Mach]

Note that the holding speeds that are used by individual aircraft may vary between types.

## 5.10 Ground Speeds

A number of ground speeds are defined for the simulation of ground movement. For the moment, no distinction between aircraft type or engine type is made. The following speeds have been defined:

<b>Name:</b>	<b>Description:</b>	<b>Value[KCAS]:</b>
$V_{backtrack}$	Runway backtrack speed	35
$V_{taxi}$	Taxi speed	15
$V_{apron}$	Apron speed	10
$V_{gate}$	Gate speed	5

The runway backtrack speed is the speed the aircraft will maintain when it backtracks across the runway. The taxi speed is used anywhere between the runway and the apron area. The apron speed is used in the apron area while the gate speed is used for all manouevering between the gate position and the apron.

## 5.11 Reduced Power Coefficient

The reduced power coefficients are defined for the three different engine types. Within the jet engines a further distinction is made between MTOWs. It is stressed that the values given below were found in an empirical way and have been validated with the help of air traffic controllers:

<b>Name:</b>	<b>Description:</b>	<b>Value[-]:</b>
$C_{red,turbo}$	Maximum reduction in power for turboprops	0.25
$C_{red,piston}$	Maximum reduction in power for pistons	0.0
$C_{red,jet}$	Maximum reduction in power for jets	0.15

The coefficients should be used in Formula 3.8-1.

## 6. FILE STRUCTURE

### 6.1 File Types

All data provided by BADA Revision 3.0 is organised into five types of files:

- two Synonym Files,
- a set of Operations Performance Files,
- a set of Airline Procedure Files,
- a set of Performance Table Files, and,
- a Global Parameter File

The two Synonym Files have the names:

SYNONYM.LST  
SYNONYM.NEW

Both files provide a list of all the aircraft types which are supported by BADA and indicate whether the aircraft type is supported directly (through provision of parameters in other files) or supported by equivalence (through indicating an equivalent aircraft type that is supported directly). The only difference between these two files is their formats which are described in Section 6.3.

There is one Operations Performance File (OPF) provided for each aircraft type which is directly supported. This file specifies parameter values for the mass, flight envelope, drag, engine thrust and fuel consumption that are described in Section 3. Details on the format of the OPF file are given in Section 6.4.

There is one Airline Procedures File (APF) for each directly supported aircraft type. This file specifies the nominal manoeuvre speeds that are described in Section 4. Details on the format of the APF file are given in Section 6.5.

There is also one Performance Table File (PTF) for each directly supported aircraft type. This file contains a summary table of speeds, climb/descent rates and fuel consumption at various flight levels. Details on the format of the PTF file are given in Section 6.6.

Finally there is one Global Parameter File which is named BADA.GPF. This file contains parameters that are described in Section 5 and are valid for all aircraft or a group of aircraft (for instance all civil flights or all jet aircraft). Details on the format of the GPF file are given in Section 6.7.

The names of the OPF, APF and PTF files are based on the ICAO designation code for the aircraft type. With the one exception of the generic military fighter aircraft type (FGTR), this code is the same as the International Civil Aviation Organisation (ICAO) designator code for the aircraft type [RD2]. That is:

Operations Performance File name: <ICAO\_code>\_\_.OPF

Airline Procedures File name: <ICAO\_code>\_\_.APF

Performance Table File name: <ICAO\_code>\_\_.PTF

Note that there are at least two underscore characters between the ICAO code and the file extension such that the length of the file name without the extension is six characters. Most ICAO codes are four characters in length and thus have two underscore characters. Some ICAO codes, however, can be shorter (e.g. DC9) and thus require more underscore characters. For example, an Airbus 310 which has the ICAO code of A310 is represented in BADA 3.0 by the following files:

Operations Performance File: A310\_\_.OPF

Airline Procedures File: A310\_\_.APF

Performance Table File: A310\_\_.PTF

The McDonnell-Douglas DC-9, which has the ICAO code of DC9 is represented in BADA 3.0 by the following files:

Operations Performance File: DC9\_\_\_\_.OPF

Airline Procedures File: DC9\_\_\_\_.APF

Performance Table File: DC9\_\_\_\_.PTF

All files belonging to BADA Revision 3.0, that is the Synonym Files, the GPF file and all APF and OPF files are controlled within a configuration management system. This system is described in Section 6.2.

## **6.2 File Configuration Management**

The BADA Synonym File and all APF and OPF files are placed under configuration management at the EEC using the UNIX-based Revision Control System (RCS). The specific procedures used for configuration management are specified in the BADA Configuration Management Manual [RD5].

The PTF files are not placed under the Revision Control System since these files are generated automatically from the OPF and APF files. The file version numbers of the OPF and APF file that were used for the calculation being are in the PTF file. Integrity of the PTF files is however traced through the recording of checksums.

Under the BADA configuration management system, users have access to the following files:

- a Revision Summary File listing all APF, OPF and PTF files contained in the revision;
- the two Synonym Files;
- the GPF file
- all APF, OPF and PTF files; and,
- all RCS files corresponding to the APF and OPF files.

Detailed instructions for remote access of the files is given in Section 7.

### **6.2.1 Revision Summary File**

The Revision Summary File provides a list of all files provided as part of the BADA Revision. The name of the Revision Summary File is simply:

revisionSummary

A copy of the Revision Summary file for BADA Revision 3.0 is included in this document as Appendix A.

The Revision Summary File lists for each file the last modification date, size in bytes and checksum.

The checksum provides a useful means to ensure that a file has not been inadvertently modified. To verify a checksum, the UNIX command **cksum** is used on the file. The first number returned is the checksum and should match the value specified in the Revision Summary File.

### **6.2.2 Revision Numbers**

All BADA Revisions are identified by a two digit number, e.g. 2.0 or 2.1. All files belonging to the BADA Revision have a file revision number which is the same as the BADA revision number.

Between releases of successive BADA Revisions, the contents of various files may be updated due to correction of coefficients, removal of excess information or addition of new information. In this case the modified file revision number is updated to a four digital number, for example:

#### **2.1.1.3**

The first two digits of the modified file revision number are the same as the last BADA Revision number in which the file was released. The third digit is always 1. The fourth digit is incremented by 1 for each successive modification of a file. It is recognised that the third digit is not necessary. This digit, however, is included for consistency with RCS numbering conventions.

Thus, if a file is modified twice between revision 2.1 and 2.2, the file revision number will undergo the following evolution:

- 2.1 - initial file revision in BADA Revision 2.1
- 2.1.1.1 - first modification
- 2.1.1.2 - second modification
- 2.2 - file released in BADA Revision 2.2, identical to 2.1.1.2.

In the Revision Summary File, the last modification date will then reflect the date on which revision 2.1.1.2 was made.

### 6.2.3 RCS Files

RCS files are files organised in a format internal to RCS which allows for the tracking of all modifications to a file.

The RCS files corresponding to the Synonym Files, GPF files or each APF or OPF file are named with a ".v" extension. For example the RCS files corresponding to B74A\_\_.OPF is:

B74A\_\_.OPF,v

These files are provided to BADA users for information purposes. The use of standard UNIX/RCS utilities such as **rlog** and **co** on these files allows for information on the file modifications to be recovered along with previous file revisions. Instructions on the use of **rlog** and **co** can be obtained from UNIX manuals.

## 6.3 Synonym File Format

### 6.3.1 SYNONYM.LST File

The SYNONYM.LST file is an ASCII file which lists all aircraft types which are supported by the BADA revision. An example of the SYNONYM.LST file is given below (partial listing).

```
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCSYNONYM.LST CCCCCCCCCCCCCC/
CC                                                 / 
CC                                                 / 
CC                                                 / 
CC      BADA RCS File Id                      / 
CC      File Name          Current Revision     Last Modification   /
CC              revision       date           revision       date   /
CC      SYNONYM.LST        3.0         98/03/12    2.6.1.5      98/03/11   /
CC                                                 / 
CC      BADA Revision:                   / 
CC                                                 / 
CD      Rev 3.0                         / 
CC===== Aircraft List ======/ 
CC                                                 / 
CC      A/C      NAME OR MODEL          FILE           SYNONYMS   /
CC      CODE                           / 
CC                                                 / 
- A300__ AIRBUS A300             A300__        A300      IL76
- A310__ AIRBUS A310             A310__        A310
- A320__ AIRBUS A320             A320__        A320
- A330__ AIRBUS A330             A330__        A330
- A340__ AIRBUS A340             A340__        A340
- ATP__  BAE ADVANCED            ATP__         ATP
TURBOPROP
- ATR__  ATR 42/72               ATR__         ATR      CN35      CVLT
- B707__ BOEING 707-300/400     B707__        B707      C135      E3
SERIES
IL62
B720
VC10
- B727__ BOEING 727,ALL SE-     B727__        B727
```

There are three types of lines in the SYNONYM.LST file with the line type identified by the first two characters in the line. These line types with their associated leading characters are listed below.

CC	comment line
CD	data line
-	synonym line

The data is organised into a two blocks separated by a comment line consisting of equal signs "=":

- file identification block; and,
- aircraft list block.

Each of these blocks is described in the subsections below.

### 6.3.1.1 File Identification Block

The file identification block provides information on the file name, revision number and modification date. The block consists of 11 comment lines and one data line.

```
ccccccccccccccccccccccccccccccccccccccccccccccccccccccccSYNONYM.LSTcccccccccccc/
CC/
CC      BADA SYNONYM FILE/
CC/
CC      BADA RCS File Id/
CC      File Name      Current Revision      Last Modification/
CC      revision       date        revision      date/
CC      SYNONYM.LST   3.0    98/03/12  2.6.1.5   98/03/11/
CC/
CC      BADA Revision:/
CC/
1 ->  CD     Rev   3.0/
```

The comment lines specify the file name along with the RCS current revision and last modification revision. For all released files, the current revision number and date will be the same as the number and date of the BADA Revision. The last modification revision number and date indicate when the contents of the file were last modified.

The data line gives the BADA Revision Id to which the file belongs. This value is specified in the following fixed format (Fortran notation):

'CD', 8X, F3.1

### 6.3.1.2 Aircraft Listing Block

The aircraft listing block consists of 5 comment lines with additional synonym lines for each aircraft supported by the BADA Revision. A partial listing of this block is shown below.

```

CC===== Aircraft List ======/  

CC  

CC A/C NAME OR MODEL FILE SYNONYMS /  

CC CODE /  

CC /  

1-> - A300__ AIRBUS A300 A300__ A300 IL76  

    - A310__ AIRBUS A310 A310__ A310  

    - A320__ AIRBUS A320 A320__ A320  

    - A330__ AIRBUS A330 A330__ A330  

    - A340__ AIRBUS A340 A340__ A340  

    - ATP__ BAE ADVANCED ATP__ ATP  

        TURBOPROP  

    - ATR__ ATR 42/72 ATR__ ATR CN35 CVLT  

    - B707__ BOEING 707-300/400 B707__ B707 C135 E3  

        SERIES IL62 VC10  

        B720

```

There is one synonym line for each of the directly supported aircraft within the BADA release. Each such line consists of 4 fields as described below:

(a) Aircraft Code Field

This field identifies the aircraft type. It consists of a three or four-character ICAO code followed by two or more underscore characters.

(b) Name or Model Field

This field identifies the manufacturer and model of the aircraft.

(c) File Name Field

This field identifies the file name for the APF, OPF or PTF files associated with the aircraft (minus the file extension). For each aircraft this is the same as the A/C code.

(d) Equivalence Field

This field lists any equivalences associated with the aircraft. By default, each aircraft has at least one equivalence to itself.

Note that in some cases the name or model or equivalence fields may be continued onto the next line as is the case with the B707.

### 6.3.2 SYNONYM.NEW File

The SYNONYM.NEW file is an ASCII file which lists all aircraft types which are supported by the BADA revision. Its format differs from the SYNONYM.LST file in that all supported aircraft are listed alphabetically in the file whether they are supported directly or by equivalence. An example of the SYNONYM.NEW file is given below (partial listing).

```
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCSYNONYM.NEW CCCCCCCCCCCCCC/
CC                                                 /
CC          BADA SYNONYM FILE                   /
CC                                                 /
CC          BADA RCS File Id                  /
CC          File Name      Current Revision    Last Modification   /
CC          revision       date             revision       date   /
CC          SYNONYM.NEW     3.0      98/03/12     2.6.1.5      98/03/11   /
CC                                                 /
CC          BADA Revision:                 /
CC                                                 /
CD          Rev 3.0                         /
CC===== Aircraft List ======/
CC          A/C      MANUFACTURER        NAME OR MODEL      FILE  OLD /   /
CC          CODE                           CODE           /   /
CC          /   /
CD * A10  FAIRCHILD        THUNDERBOLT II      FGTR__ A10A  /
CD - A300 AIRBUS            A300              A300__ EA30  /
CD - A310 AIRBUS            A310              A310__ EA31  /
CD - A320 AIRBUS            A320              A320__ EA32  /
CD - A330 AIRBUS            A330              A330__ EA33  /
CD - A340 AIRBUS            A340              A340__ EA34  /
CD * A4   MCDONNELL-DOUGLAS SKYHAWK          FGTR__ A4   /
CD * A6   GRUMMAN            INTRUDER          FGTR__ A6   /
CD * AC6T ROCKWELL          TURBO COMMANDER  BE20__ AC6T  /
CD * AN12 ANTONOV          AN-12             C130__ AN12  /
CD * AN24 ANTONOV          AN-24             F27__  AN24  /
CD * AN26 ANTONOV          AN-26             F27__  AN26  /
CD - ATP  BAE               ADVANCED TURBOPROP ATP__  BATP  /
CD - ATR  ATR               ATR 42/72         ATR__  AT42  /
CD - ATR  ATR               ATR 42/72         ATR__  AT72  /
CD - B707 BOEING            707-300/400     B707__ B707  /
CD * B720 BOEING            720B             B707__ B72S  /
CD - B727 BOEING            727, ALL SERIES B727__ B727  /
```

There are three types of lines in the SYNONYM.NEW file with the line type identified by the first two characters in the line. These line types with their associated two leading characters are listed below.

CC comment line

CD data line

FI end-of-file line.

The data is organised into a two blocks separated by a comment line consisting of equal signs "=":

- file identification block; and,
- aircraft list block.

Each of these blocks is described in the subsections below.

### 6.3.2.1 File Identification Block

The file identification block provides information on the file name, revision number and modification date. The block consists of 1 data line with 11 comment lines for a total of 12 lines as shown below.

```
ccccccccccccccccccccccccccccccccccccccccccccccccccccccccSYNONYM.NEWcccccccccccc/
CC                                                 /
CC          BADA SYNONYM FILE                   /
CC                                                 /
CC          BADA RCS File Id                     /
CC          File Name      Current Revision    Last Modification   /
CC          revision       date                 revision       date   /
CC          SYNONYM.NEW  3.0        98/03/12     2.6.1.5      98/03/11   /
CC                                                 /
CC          BADA Revision:                      /
CC                                                 /
1 ->      CD      Rev  3.0                         /
```

The only data line gives the BADA Revision Id to which the file belongs. This value is specified in the following fixed format (Fortran notation):

'CD', 8X, F3.1

The comment lines specify the file name along with the RCS current revision and last modification revision. For all released files, the current revision number and date will be the same as the number and date of the BADA Revision. The last modification revision number and date indicate when the contents of the file were last modified.

### 6.3.2.2 Aircraft Listing Block

The aircraft listing block consists of 5 comment lines and at least one data line for each aircraft supported by the BADA Revision. Some aircraft have more than one data line, see under (f). A partial listing of this block is shown below.

CD - A330	AIRBUS	A330	A330	EA33	/
CD - A340	AIRBUS	A340	A340	EA34	/
CD * A4	MCDONNELL-DOUGLAS	SKYHAWK	FGTR	A4	/
CD * A6	GRUMMAN	INTRUDER	FGTR	A6	/

Each data line consists of 5 fields as described below:

(a) Support Type Field

This field is one character in length being one of the following two values:

- "\_" to indicate an aircraft type directly supported, and,
- "\*" to indicate an aircraft type supported by equivalence with another directly supported aircraft

## (b) Aircraft Code Field

This field identifies the aircraft type. It consists of a three or four-character ICAO code.

## (c) Manufacturer Field

This field identifies the manufacturer of the aircraft. Examples are Boeing, Airbus or Fokker.

## (d) Name or Model Field

This field identifies the name or model for the aircraft type. Examples are the 747-400 series or Learjet 35.

## (e) File Field

This field indicates the name of the OPF, APF or PTF file which contains the parameters for the aircraft type (minus the file extension).

For an aircraft type which is directly supported this file name will be the same as the ICAO code with an additional two or more underscore characters to form a string of six characters in length. For example, the file name corresponding to the B707 will be B707\_\_. This indicates an OPF file B707\_\_.OPF, an APF file B707\_\_.APF and a PTF file B707\_\_.PTF. For the Fokker F-27 with an ICAO code of F27, the file names include three underscore characters, that is, F27\_\_\_\_.OPF, F27\_\_\_\_.APF and F27\_\_\_\_.PTF.

For an aircraft type which is supported through an equivalence, the file name will indicate the file for the equivalent aircraft type which should be used. As an example, the Antonov 12 (AN12) is equivalenced to the Lockheed C-130 Hercules (C130). Thus the files C130\_\_.OPF, C130\_\_.APF and C130\_\_.PTF should be used.

## (f) Old Code field

The old code field gives the name of the aircraft under the old ICAO standard (doc. 8643/24) [RD10]. This allows the BADA 3.0 user to continue to use the old standard and to establish a link between the old and the new aircraft designators. For this reason some aircraft types now appear more than once (ATR, B73B and DHC8) because under the old standard these aircraft were covered by more than one designator (e.g. ATR used to be AT42 and AT72).

The above fields are specified in the following fixed format (Fortran notation):

'CD', 1X, A1, 1X, A4, 3X, A18, 1X, A25, 1X, A6, 2X, A4

## 6.4 OPF File Format

The Operations Performance File (OPF) is an ASCII file, which for a particular aircraft type specifies the operations performance parameters described in Section 3. An example of an OPF file for the A320 (Airbus 320) aircraft is shown below.

```

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC A320__.OPF CCCCCCCCCCCCCCCC/
CC /
CC           AIRCRAFT PERFORMANCE /
CC           operational files /
CC /
CC   BADA RCS File Id /
CC   File Name      Current Revision      Last Modification /
CC   revision date   revision date /
CC   A320__.OPF      3.0    98/03/12    2.6.1.1    98/03/11 /
CC /
CC   BADA Revision: /
CD   Rev 3.0 /
CC===== Actype =====/
CD   A320__ 2 engines Jet M /
CC   Airbus A320-111 with CFM56_5_A1 engines wake /
CC   (source: AIR FRANCE OPS manual) /
CC===== Mass (t) =====/
CC   reference minimum maximum max payload mass grad /
CD   .62000E+02  .41800E+02  .73500E+02  .19220E+02  .32000E+00 /
CC===== Flight envelope =====/
CC   VMO(KCAS)     MMO     Max.Alt   Hmax   temp grad /
CD   .35000E+03  .82000E+00  .39000E+05  .36500E+05  -.40000E+02 /
CC===== Aerodynamics =====/
CC Wing Area and Buffet coefficients (SIM) /
CCnldrst Surf(m2)  Clbo(M=0) k CM16 /
CD 5  .12240E+03  .12100E+01  .47000E+00  .00000E+00 /
CC Configuration characteristics /
CC n Phase Name Vstall(KCAS) CD0 CD2 unused /
CD 1 CR Clean  .14700E+03  .20000E-01  .40000E-01  .00000E+00 /
CD 2 IC 1+F  .11700E+03  .00000E+00  .00000E+00  .00000E+00 /
CD 3 TO 1+F  .11700E+03  .00000E+00  .00000E+00  .00000E+00 /
CD 4 AP 2  .10900E+03  .42000E-01  .34000E-01  .00000E+00 /
CD 5 LD FULL  .10500E+03  .74000E-01  .35000E-01  .00000E+00 /
CC Spoiler /
CD 1 RET /
CD 2 EXT  .00000E+00  .00000E+00 /
CC Gear /
CD 1 UP /
CD 2 DOWN  .24000E-01  .00000E+00  .00000E+00 /
CC Brakes /
CD 1 OFF /
CD 2 ON  .00000E+00  .00000E+00 /
CC===== Engine Thrust =====/
CC   Max climb thrust coefficients (SIM) /
CD   .12900E+06  .48900E+05  .71100E-10  .00000E+00  .15000E-02 /
CC   Desc(low) Desc(high) Desc level Desc(app) Desc(lid) /
CD   -.20000E-01  -.90000E-01  .20000E+05  .13000E+00  .30000E+00 /
CC   Desc CAS Desc Mach unused unused unused /
CD   .30000E+03  .78000E+00  .00000E+00  .00000E+00  .00000E+00 /
CC===== Fuel Consumption =====/
CC   Thrust Specific Fuel Consumption Coefficients /
CD   .10000E+01  .50000E+05 /
CC   Descent Fuel Flow Coefficients /
CD   .94000E+01  .90000E+05 /
CC   Cruise Corr. unused unused unused unused /
CD   .10950E+01  .00000E+00  .00000E+00  .00000E+00  .00000E+00 /
CC===== Ground =====/
CC   TOL LDL span length unused /
CD   .21900E+04  .14400E+04  .34100E+02  .37570E+02  .00000E+00 /
CC===== FI =====/
FI

```



The only data line gives the BADA Revision Id to which the file belongs. This value is specified in the following fixed format (Fortran notation):

'CD', 8X, F3.1

The comment lines specify the file name along with the RCS current revision and last modification revision. For all released files, the current revision number and date will be the same as the number and date of the BADA Revision. The last modification revision number and date indicate when the contents of the file were last modified.

#### 6.4.2 Aircraft Type Block

The OPF aircraft type block consists of 1 data line with 3 comments lines for a total of 4 lines. An example of the aircraft type block is given below.

```
CC===== Actype ======/  
1 -> CD EA32__ 2 engines Jet M /  
CC Airbus A320-111 with CFM56_5_A1 engines wake /  
CC (source: AIR FRANCE OPS manual) /
```

The data line specifies the following aircraft type parameters:

- ICAO aircraft code  
(followed by 2 or more underscore characters as required to form a six character string),
- number of engines,  $n_{eng}$ ,
- engine type, and,
- wake category

The engine type can be one of the following three values: Jet, Turboprop or Piston. The wake category can be one of the three values H (heavy), M (medium) or L (light).

The four values are specified in the following fixed format (Fortran notation)

'CD', 2X, A6, 10X, I1, 12X, A9, 17X , A1

The comment lines typically indicate the engine manufacturer's designation and the source of the performance coefficients.

#### 6.4.3 Mass Block

The OPF mass block consists of 1 data line with 2 comment lines for a total of 3 lines. An example of the mass block is given below.

```
CC===== Mass (t) ======/  
CC reference minimum maximum max payload mass grad /  
1 -> CD .62000E+02 .41800E+02 .73500E+02 .19220E+02 .32000E+00 /
```

The data line specifies the following BADA mass model parameters (in tonnes):

m <sub>ref</sub>	m <sub>min</sub>	m <sub>max</sub>	m <sub>pyld</sub>	G <sub>w</sub>
------------------	------------------	------------------	-------------------	----------------

These parameters are specified in the following fixed format (Fortran notation)

'CD', 2X, 5( 3X, E10.5 )

#### 6.4.4 Flight Envelope Block

The OPF flight envelope block consists of 1 data line with 2 comment lines for a total of 3 lines. An example of the flight envelope block is given below.

```
CC===== Flight envelope =====/
CC      VMO(KCAS)      MMO      Max.Alt      Hmax      temp grad /
1 -> CD      .35000E+03   .82000E+00   .39000E+05   .36500E+05  -.40000E+02 /
```

The date line specifies the following BADA speed envelope parameters:

V <sub>MO</sub>	M <sub>MO</sub>	h <sub>MO</sub>	h <sub>max</sub>	G <sub>t</sub>
-----------------	-----------------	-----------------	------------------	----------------

Note that all altitudes are expressed in feet.

These parameters are specified in the following fixed format (Fortran notation):

'CD', 2X, 5( 3X, E10.5 )

#### 6.4.5 Aerodynamics Block

The OPF aerodynamics block consists of 12 data lines and 8 comment lines for a total of 20 lines. An example of the aerodynamics block is given below.

```
CC===== Aerodynamics =====/
CC Wing Area and Buffet coefficients (SIM) /
CCn drst Surf(m2) Clbo(M=0) k CM16 /
1 -> CD 5 .12240E+03 .00000E+00 .00000E+00 .00000E+00 /
CC Configuration characteristics /
CC n Phase Name Vstall(KCAS) CDO CD2 unused /
2 -> CD 1 CR Clean .14700E+03 .20000E-01 .40000E-01 .00000E+00 /
3 -> CD 2 IC 1+F .11700E+03 .00000E+00 .00000E+00 .00000E+00 /
4 -> CD 3 TO 1+F .11700E+03 .00000E+00 .00000E+00 .00000E+00 /
5 -> CD 4 AP 2 .10900E+03 .42000E-01 .34000E-01 .00000E+00 /
6 -> CD 5 LD FULL .10530E+03 .74000E-01 .35000E-01 .00000E+00 /
CC Spoiler /
7 -> CD 1 RET /
8 -> CD 2 EXT .00000E+00 .00000E+00 /
CC Gear /
9 -> CD 1 UP /
10 -> CD 2 DOWN .24000E-01 .00000E+00 .00000E+00 /
CC Brakes /
11 -> CD 1 OFF /
12 -> CD 2 ON .00000E+00 .00000E+00 /
```

The first data line specifies the following BADA aerodynamic model parameters:

S	Clbo(M=0)	k	C <sub>M16</sub>
---	-----------	---	------------------

These parameters are specified in the following fixed format (Fortran notation):

'CD', 2X, 4 (3X, E10.5)

Note that the "5" under the header "ndrst" stands for the five drag settings. Currently this is not used but is left in for compatibility requirements.

The next line holds besides the stall speed and flap setting for cruise as well as the values for the two drag coefficients for this configuration:

$(V_{stall})_{CR}$        $C_{D0}$        $C_{D2}$

These parameters are specified in the following fixed format (Fortran notation):

'CD', 15X, 3 (3X, E10.5)

The next four data lines have the same format and correspond to the other configurations. The configurations are specified in the following order, corresponding to a semi-monotonically decreasing stall speed:

IC	initial climb
TO	take-off
AP	approach
LD	landing

The stall speed,  $(V_{stall})_i$ , is specified for each configuration and  $C_{D0}$  and  $C_{D2}$  are given if available in the following fixed format (Fortran notation):  $C_{D0}$  and  $C_{D2}$

'CD', 15X, 3 (3X, E10.5)

In case the IC configuration is equal to the CR configuration, the values for  $C_{D0}$  and  $C_{D2}$  are mentioned only in the CR dataline. Note that in BADA 3.0 only 9 models have values for the  $C_{D0}$  and  $C_{D2}$  coefficients for approach and landing and that dragsettings for take-off and initial climb are not used at all.

The data lines 7 through 9 are not used but are included for the reason of compatibility with previous versions.

Dataline 10 holds the drag increment for landing gear down:

$C_{D0\ ALDG}$

The format of this line is:

'CD', 32X, E10.5

Datalines 11 and 12 are not used but are included for the reason of compatibility with previous versions.

### 6.4.6 Engine Thrust Block

The OPF engine thrust block consists of 3 data lines with 4 comment lines for a total of 7 lines. An example of the engine thrust block is given below.

```
CC===== Engine Thrust =====/
CC      Max climb thrust coefficients (SIM) /
1 -> CD    .12900E+06   .48900E+05   .71100E-10   .00000E+00   .15000E-02 /
2 -> CD    Desc(low)   Desc(high)   Desc level   Desc(app)   Desc(ld)   /
2 -> CD    -.20000E-01  -.90000E-01  .20000E+05  .13000E+00  .30000E+00 /
3 -> CD    Desc CAS    Desc Mach    unused       unused       unused   /
3 -> CD    .30000E+03   .78000E+00   .00000E+00   .00000E+00   .00000E+00 /
```

The first data line specifies the following BADA parameters used to calculate the maximum climb thrust, that is:

$C_{Tc,1}$        $C_{Tc,2}$        $C_{Tc,3}$        $C_{Tc,4}$        $C_{Tc,5}$

These parameters are specified in the following fixed format (Fortran notation):

'CD', 2X, 5 (3X, E10.5)

The second data line specifies the following BADA parameters used to calculate cruise and descent thrust, that is:

$C_{Tdes,low}$        $C_{Tdes,high}$        $h_{des}$        $C_{Tdes,app}$        $C_{Tdes,ld}$

These parameters are specified in the following fixed format (Fortran notation):

'CD', 2X, 5 (3X, E10.5)

The third data line specifies the reference speed during descent, that is:

$V_{des,ref}$        $M_{des,ref}$

These parameters are specified in the following fixed format (Fortran notation):

'CD', 2X, 2 (3X, E10.5)

Note that these two coefficients are no longer used in BADA 3.0. For the moment they are left in place until it is clear if they will be of use for the new descent thrust algorithm, to be developed for a future release of BADA.

The zero values in the data lines are not used but are included in the file due to compatibility requirements with previous versions.

### 6.4.7 Fuel Consumption Block

The OPF fuel consumption block consists of 3 data lines with 4 comment lines for a total of 7 lines. An example of a fuel consumption block is shown below.

```

CC===== Fuel Consumption =====/
CC   Thrust Specific Fuel Consumption Coefficients /
1 -> CD   .10000E+01   .50000E+05   /
CC   Descent Fuel Flow Coefficients /
2 -> CD   .94000E+01   .90000E+05   /
CC   Cruise Corr.    unused    unused    unused    unused   /
3 -> CD   .10950E+01   .00000E+00   .00000E+00   .00000E+00   .00000E+00   /

```

The first data line specifies the following BADA parameters for thrust specific fuel consumption.

$C_{f1}$        $C_{f2}$

These parameters are specified in the following fixed format (Fortran notation):

'CD', 2X, 2 (3X, E10.5)

The second data line specifies the following BADA parameters for descent fuel flow.

$C_{f3}$        $C_{f4}$

These parameters are specified in the following fixed format (Fortran notation):

'CD', 2X, 2 (3X, E10.5)

The third data line specifies the cruise fuel flow correction factor.

$C_{fcr}$

The parameter is specified in the following fixed format (Fortran notation):

'CD', 5X, E10.5

#### 6.4.8 Ground Movement Block

The OPF ground movement block consists of 1 data line with 3 comment lines for a total of 4 lines. An example of a ground movement block is shown below. The ground movement block is the last block in the OPF file and is thus followed by the end-of-file line as shown below.

```

CC===== Ground =====/
CC      TOL      LDL      span      length      unused   /
1 -> CD   .21900E+04   .14400E+04   .34100E+02   .37570E+02   .00000E+00   /
CC===== /
FI

```

The dataline specifies the following BADA parameters for ground movements:

$TOL$        $LDL$        $span$        $length$

These parameters are specified in the following fixed format (Fortran notation):

'CD', 2X, 4 (3X, E10.5)

## 6.5 APF File Format

The Airlines Procedures File (APF) is an ASCII file which, for a particular aircraft type, specifies recommended speed procedures for climb, cruise, and descent conditions. An example of an APF file for the Boeing 767 aircraft is shown below.

```
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC /  
CC                                         /  
CC      AIRLINES PROCEDURES FILE           /  
CC                                         /  
CC      File Name          Current Revision          Last Modification    /  
CC                  revision    date           revision    date       /  
CC      B767__.APF          3.0     98/03/12      2.4.1.2     96/09/05     /  
CC                                         /  
CC      BADA Revision:       /  
CD      Rev 3.0              /  
CC                                         /  
CC      LO= 90.00 to ---.-- / AV= ---.-- to ---.-- / HI= ---.-- to 181.40 /  
CC                                         /  
CC======  
CC      COM CO    Company name -----climb----- --cruise-- -----descent----- --approach- model- /  
CC              mass lo hi        lo hi       hi lo             (unused)          /  
CC      version engines ma cas cas mc xxxx xx cas cas mc mc cas cas xxxx xx xxx xxx xxx opf__ /  
CC======  
CD      *** * * Default Company          /  
CD      300ER   PW4060  LO 290 290 78        310 310 80  78 290 290           0   0   0  B767__ /  
CD      300ER   PW4060  AV 290 290 78        310 310 80  78 290 290           0   0   0  B767__ /  
CD      300ER   PW4060  HI 290 290 78        310 310 80  78 290 290           0   0   0  B767__ /  
CC======  
CC//THE END //////////////////////////////////////////////////////////////////// THE END ////////////////////////////////////////////////////////////////////
```

There are two types of lines in the APF file with the line type identified by the first two characters in the line. These line types with their associated two leading characters are listed below:

- CC - comment line
- CD - data line

The last line in the file, as shown above, is also a comment line.

The comment lines are provided solely for the purpose of improving the readability of the file. All coefficients are contained within the CD lines in a fixed format.

The data is organised into 2 blocks separated by a comment line containing a string of equal signs, "=":

- file identification block, and,
- speed procedures block.

Each of the two blocks is described further in the subsections below.

### 6.5.1 File Identification Block

The file identification block provides information on the file name, revision number and modification date. The block consists of 1 data line with 12 comment lines for a total of 13 lines. An example of a file identification block is shown below.

```

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC B767__.APF CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC /  

CC /  

CC AIRLINES PROCEDURES FILE /  

CC /  

CC File Name Current Revision Last Modification /  

CC revision date revision date /  

CC B767__.APF 3.0 98/03/12 2.4.1.2 96/09/05 /  

CC /  

CC BADA Revision: /  

1-> CD Rev 3.0 /  

CC /  

CC LO= 90.00 to ---.-- / AV= ---.-- to ---.-- / HI= ---.-- to 181.40 /  

CC /

```

The only data line gives the BADA Revision Id to which the file belongs. This value is specified in the following fixed format.

'CD', 8X, F3.1

The comment lines provide background information on the file contents. In addition, the comment lines specify the file name along with the RCS current revision and last modification. For all released files, the current revision number and date are the same as the number and date of the BADA revision. The last modification revision number and date indicate when the contents of the file were last modified.

The second last comment line in the identification block specifies three mass ranges for the aircraft in tonnes. That is, a low range (LO), average range (AV) and high range (HI). The definition of these ranges is used for interpreting the information presented below in the procedures specification block. In the example given above, all three ranges are assumed equivalent.

## 6.5.2 Procedures Specification Block

The APF procedures specification block consists of 4 data lines with 7 comment lines for a total of 11 lines. An example of a procedures specification block is shown below.

```

CC===== /  

CC COM CO Company name ----climb---- --cruise-- ----descent---- --approach- model- /  

CC mass lo hi lo hi hi lo (unused) /  

CC version engines ma cas cas mc xxxx xx cas cas mc mc cas cas xxxx xx xxx xxx xxxx opf__ /  

CC====:====:====:====:====:====:====:====:====:====:====:====:====:====:====:====:====:====:====: /  

1-> CD *** ** Default Company /  

2-> CD 300ER PW4060 LO 290 290 78 310 310 80 78 290 290 0 0 0 B767__ /  

3-> CD 300ER PW4060 AV 290 290 78 310 310 80 78 290 290 0 0 0 B767__ /  

4-> CD 300ER PW4060 HI 290 290 78 310 310 80 78 290 290 0 0 0 B767__ /  

CC====:====:====:====:====:====:====:====:====:====:====:====:====:====:====:====:====:====:====: /  

CC////////// THE END ////////// /  


```

The first data line specifies the company name for which the next three datalines are valid. The company can be identified by its 3 and 2 letter code plus the company name. The dataline fomat is:

'CD', 2X, 3A, 1X, 2A, 4X, 15A

As it is, within BADA 3.0 all APF files specify procedures for only one "default" company.

The next three data lines specify the following parameters corresponding to climb, cruise and descent

$V_{cl,1}$	$V_{cl,2}$	$M_{cl}$	$V_{cr,1}$	$V_{cr,2}$	$M_{cr}$	$M_{des}$	$V_{des,1}$	$V_{des,2}$
------------	------------	----------	------------	------------	----------	-----------	-------------	-------------

Note that all Mach numbers values are also multiplied by a value of 100. For example, the 78 indicated for  $M_{cl}$  above corresponds to a Mach number of 0.78.

The three lines specify parameters for mass ranges of Low (LO), Average (AV) and High (HI) respectively. These parameters are specified in the following fixed format (Fortran notation):

'CD', 25X, 2(I3, 1X), I2, 10X, 2(I3, 1X), I2, 2X, I2, 2(1X, I3)

Note that approach values are set to zero. These values are not used but are included in the file due to compatibility requirements with previous versions.

Also each line specifies an aircraft version number, engine, and operational model. The operational model is always the same as the file name. The version number may provide some additional information on the aircraft version covered by the file while the engine states which engine is used by the aircraft.

The file format is designed such that the four data lines can be repeated for the different companies which operate the aircraft and which may have different standard procedures. If data were to be provided for more than one company then the version, engine and operational model fields may be useful since different companies could operate different versions of the aircraft with different engines and thus different associated operational models.

## 6.6 PTF File Format

The Performance Table File (PTF) is an ASCII file, which for a particular aircraft type specifies cruise, climb and descent performance at different flight levels. An example of a PTF file for the Fokker F-28 aircraft (F28) is shown below.

BADA PERFORMANCE FILE									98/03/12			
AC/Type: F28		Last BADA Revision: 3.0				Source OPF File: 3.0 98/03/12						
		Source APF file: 3.0 98/03/12										
Speeds: CAS(LO/HI)		Mach	Mass Levels [kg]				Temperature: ISA					
climb -	250/270	0.65	low	-	20880							
cruise -	250/300	0.70	nominal	-	24000	Max Alt. [ft]: 35000						
descent -	250/280	0.70	high	-	33000							
FL	CRUISE				CLIMB			DESCENT				
	TAS [kts]	fuel [kg/min]			TAS [kts]	ROCD [fpm]	fuel [kg/min]	TAS [kts]	ROCD [fpm]	fuel [kg/min]		
		lo	nom	hi		lo	nom	hi	nom	nom		
0					127	2760	2860	2370	108.1	108	900	19.5
5					128	2710	2820	2330	106.4	108	910	19.5
10					129	2670	2780	2290	104.6	114	890	19.4
15					135	2800	2880	2360	103.3	125	850	19.4
20					136	2760	2830	2320	101.6	157	820	19.4
30	261	19.5	20.8	25.8	159	3270	3260	2650	100.0	230	1070	19.3
40	265	19.5	20.9	25.8	193	3960	3820	3070	99.3	233	1080	19.2
60	272	19.6	21.0	26.0	272	5170	4570	3410	98.3	240	1110	19.1
80	280	19.7	21.1	26.1	280	4810	4250	3140	91.7	280	1380	19.0
100	289	19.8	21.2	26.3	289	4460	3930	2880	85.4	289	1410	18.8
120	356	26.4	27.4	31.2	321	4220	3720	2730	80.9	332	1770	18.7
140	366	26.5	27.5	31.3	330	3860	3390	2460	75.1	342	1810	18.6
160	377	26.5	27.6	31.5	340	3500	3060	2200	69.7	353	1840	18.4
180	388	26.6	27.7	31.6	351	3150	2750	1940	64.6	363	1870	18.3
200	400	26.7	27.8	31.8	362	2820	2450	1690	59.8	375	1900	18.1
220	412	26.8	27.9	31.9	373	2510	2160	1460	55.3	386	1930	18.0
240	423	26.6	27.7	31.9	385	2210	1890	1230	51.2	398	1950	17.9
260	419	24.9	26.1	30.7	389	2500	2120	1320	47.1	411	1980	17.7
280	416	23.4	24.8	29.7	386	2210	1850	1070	43.2	416	2570	17.6
300	412	22.1	23.6	29.0	383	1950	1600	840	39.7	412	2430	17.5
320	408	20.9	22.6	28.5	379	1710	1380	630	36.6	408	1890	17.3
340	405	20.0	21.7	28.2	376	1510	1180	430	34.0	405	1830	17.2
360	401	19.1	21.1	28.2	372	1330	1010	240	31.7	401	1780	17.1
380	401	18.6	20.7	28.5	372	1120	810	70	29.9	401	1640	16.9
400	401	18.1	20.5	27.7	372	1010	690	0	28.5	401	1640	16.8

The OPF and APF files are generated as a result of a modelling process using Excel spreadsheets [RD6]. Once these two files are generated, the PTF can be automatically generated. A brief summary of the format of these files is given below.

The header of each PTF file contains information as described below.

file creation date: This is in the first line, at the top-right corner

aircraft type: This is in the third line.

last BADA revision: This is in the 3rd line and indicates the last BADA revision which has been released as of the file creation date.

source file revisions: The RCS revision numbers and dates of the OPF and APF files which were used to create the PTF file are given in the 4th and 5th lines respectively.

speeds: The speed laws for climb, cruise and descent are specified in lines 8, 9 and 10, that is:

climb	$V_{cl,1} / V_{cl,2}$	$M_{cl}$
cruise	$V_{cr,1} / V_{cr,2}$	$M_{cr}$
descent	$V_{des,1} / V_{des,2}$	$M_{des}$

mass Levels: The performance tables provide data for three different mass levels in lines 8, 9 and 10 that is:

low	$1.2 m_{min}$
nominal	$m_{ref}$
high	$m_{max}$

temperature: The temperature is mentioned in line 7. All PTF files currently only provide data for ISA conditions.

maximum altitude: The maximum altitude as specified in the OPF file,  $h_{MO}$ , is given in line 9.

The table of performance data within the file consists of 13 columns. Each of these columns is described below:

Column 1	FL
Column 2	cruise TAS (nominal mass) in knots
Column 3	cruise fuel consumption (low mass) in kg/min
Column 4	cruise fuel consumption (nominal mass) in kg/min
Column 5	cruise fuel consumption (high mass) in kg/min
Column 6	climb TAS (nominal mass) in knots
Column 7	rate of climb with reduced power (low mass) in fpm
Column 8	rate of climb with reduced power (nominal mass) in fpm
Column 9	rate of climb with reduced power (high mass) in fpm
Column 10	climb fuel consumption in kg/min
Column 11	descent TAS (nominal mass) in knots
Column 12	rate of descent (nominal mass) in fpm
Column 13	descent fuel (nominal mass) consumption in fpm

The format for data presented in each line of the table is as follows (Fortran notation)

I3, 4X, I3, 2X, 3(2X, F4.1), 5X, I3, 2X, 3(1X,I4), 4X, F4.1, 5X, I3, 2X, I4, 4X, F4.1

Further explanatory notes on the data presented in the performance tables are given below:

- (a) Cruise data is only specified for flight levels greater than or equal to 30.
- (b) Performance data is specified up to a maximum flight level of 400 or to highest level for which a positive rate of climb can be achieved at the low mass. This maximum level is not necessarily the same as the maximum level specified in the OPF file and given in the PTF header.
- (c) True Air Speed for climb, cruise and descent is determined based on the speed schedules specified in Sections 4.1, 4.2 and 4.3 respectively.
- (d) Rates of climb are calculated at each flight level assuming the energy share factors associated with constant CAS or constant Mach speed laws and using the reduced power correction as given in Section 3.8.
- (e) The fuel consumption in climb is independent of the aircraft mass and thus only one value is given. There are three different climb rates however corresponding to low, nominal and high mass conditions.
- (f) The rate of descent and fuel consumption in descent is calculated assuming the nominal mass. Values for other mass conditions are not given.
- (g) Discontinuities in climb rate can occur for the following reasons:
  - change in speed between flight levels (e.g. removal of 250 knot restriction above FL100)
  - transition from constant CAS to constant Mach (typically around FL300)
  - transition through the tropopause (FL360 for ISA)
- (h) Discontinuities in descent rate can occur for the following reasons:
  - transition through tropopause (FL360 for ISA)
  - transition from constant Mach to constant CAS
  - change in assumed descent thrust (specified by the BADA  $h_{des}$  parameter)
  - change in speed between flight levels (e.g. application of 250 knot limit below FL100)
- (i) The PTF files are made with "clean" configuration data only.

Note that all PTF files are available in document form in [RD9].

## 6.7 BADA.GPF File Format

The BADA.GPF file is an ASCII file which specifies the values of the global aircraft parameters (see Section 5). The complete BADA.GPF file is shown below:

```
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC BADA.GPF CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC  

CC /  

CC GLOBAL PARAMETERS FILE /  

CC /  

CC BADA RCS File Id /  

CC File Name Current Revision Last Modification /  

CC revision date revision date /  

CC BADA.GPF 3.0.1.1 98/03/13 3.0.1.1 98/03/13 /  

CC /  

CC BADA Revision: /  

CC /  

CD Rev 3.0 /  

CC===== Class ======/  

CC /  

CC Flight = civ,mil /  

CC Engine = jet,turbo,piston /  

CC Phase = to,ic,cl,cr,des,hold,app,lnd,gnd /  

CC /  

CC===== Parameters List ======/  

CC /  

CC Name Unit /  

CC Parameter Flight Engine Phase Value /  

CC /  

CC max. long. acc. [fps2] /  

CD acc_long_max civ jet,turbo,piston to,ic,cl,cr,des,hold,app,lnd .20000E+01 /  

CC max. norm. acc. [fps2] /  

CD acc_norm_max civ jet,turbo,piston to,ic,cl,cr,des,hold,app,lnd .50000E+01 /  

CC nom. bank angle [deg] /  

CD ang_bank_nom civ jet,turbo,piston to,lnd .15000E+02 /  

CC nom. bank angle [deg] /  

CD ang_bank_nom civ jet,turbo,piston ic,cl,cr,des,hold,app .35000E+02 /  

CC nom. bank angle [deg] /  

CD ang_bank_nom mil jet,turbo,piston to,ic,cl,cr,des,hold,app,lnd .50000E+02 /  

CC max. bank angle [deg] /  

CD ang_bank_max civ jet,turbo,piston to,lnd .25000E+02 /  

CC max. bank angle [deg] /  

CD ang_bank_max civ jet,turbo,piston hold .30000E+02 /  

CC max. bank angle [deg] /  

CD ang_bank_max civ jet,turbo,piston ic,cl,cr,des,app .45000E+02 /  

CC max. bank angle [deg] /  

CD ang_bank_max mil jet,turbo,piston to,ic,cl,cr,des,hold,app,lnd .70000E+02 /  

CC exp. desc. fact. [-] /  

CD C_des_exp civ,mil jet,turbo,piston des .16000E+01 /  

CC to thrust factor [-] /  

CD C_th_to mil,civ jet,turbo,piston to .12000E+01 /  

CC cr thrust factor [-] /  

CD C_th_cr mil,civ jet,turbo,piston cr .95000E+00 /  

CC max alt for to [ft] /  

CD H_max_to mil,civ jet,turbo,piston to .40000E+03 /  

CC max alt for ic [ft] /  

CD H_max_ic mil,civ jet,turbo,piston ic .20000E+04 /  

CC max alt for app [ft] /  

CD H_max_app mil,civ jet,turbo,piston app .80000E+04 /  

CC max alt for ld [ft] /  

CD H_max_ld mil,civ jet,turbo,piston lnd .30000E+04 /  

CC min speed coef. [-] /  

CD C_v_min mil,civ jet,turbo,piston cr,ic,cl,des,hold,app,lnd .13000E+01 /  

CC min speed coef. [-] /  

CD C_v_min_to mil,civ jet,turbo,piston to .12000E+01 /  

CC spd incr FL < 15 [KCAS] /  

CD V_cl_1 mil,civ jet cl .50000E+01 /  

CC spd incr FL < 30 [KCAS] /  

CD V_cl_2 mil,civ jet cl .10000E+02 /  

CC spd incr FL < 40 [KCAS] /  

CD V_cl_3 mil,civ jet cl .30000E+02 /  

CC spd incr FL < 50 [KCAS] /  

CD V_cl_4 mil,civ jet cl .60000E+02 /  

CC spd incr FL < 60 [KCAS] /  

CD V_cl_5 mil,civ jet cl .80000E+02 /  

CC spd incr FL < 5 [KCAS] /  

CD V_cl_6 mil,civ turbo,piston cl .20000E+02 /  

CC spd incr FL < 10 [KCAS] /  

CD V_cl_7 mil,civ turbo,piston cl .30000E+02 /  

CC spd incr FL < 15 [KCAS] /  

CD V_cl_8 mil,civ turbo,piston cl .35000E+02 /  

CC spd incr FL < 10 [KCAS] /  

CD V_des_1 mil,civ jet,turbo des .50000E+01 /  

CC spd incr FL < 15 [KCAS] /  

CD V_des_2 mil,civ jet,turbo des .10000E+02 /  

CC spd incr FL < 20 [KCAS] /  

CD V_des_3 mil,civ jet,turbo des .20000E+02 /
```

## (BADA.GPF continued)

```

CC spd incr FL < 30 [KCAS] /
CD V_des_4      mil,civ jet,turbo      des   .50000E+02 /
CC spd incr FL < 5  [KCAS] /
CD V_des_5      mil,civ piston      des   .50000E+01 /
CC spd incr FL < 10 [KCAS] /
CD V_des_6      mil,civ piston      des   .10000E+02 /
CC spd incr FL < 15 [KCAS] /
CD V_des_7      mil,civ piston      des   .20000E+02 /
CC hold. spd FL < 140 [KCAS] /
CD V_hold_1     mil,civ jet,turbo,piston hold .23000E+03 /
CC hold. spd FL < 200 [KCAS] /
CD V_hold_2     mil,civ jet,turbo,piston hold .24000E+03 /
CC hold. spd FL < 340 [KCAS] /
CD V_hold_3     mil,civ jet,turbo,piston hold .26500E+03 /
CC hold. spd FL > 340 [M] /
CD V_hold_4     mil,civ jet,turbo,piston hold .83000E+00 /
CC backtrack spd [KCAS] /
CD V_backtrack  mil,civ jet,turbo,piston gnd .35000E+02 /
CC taxi spd    [KCAS] /
CD V_taxi       mil,civ jet,turbo,piston gnd .15000E+02 /
CC apron spd   [KCAS] /
CD V_apron      mil,civ jet,turbo,piston gnd .10000E+02 /
CC gate spd    [KCAS] /
CD V_gate       mil,civ jet,turbo,piston gnd .50000E+01 /
CC Piston pow. red. [-] /
CD C_red_piston mil,civ piston      ic,cl .000000+00 /
CC Turbo pow. red. [-] /
CD C_red_turbo  mil,civ turbo      ic,cl .250000+00 /
CC Jet power red. [-] /
CD C_red_jet   mil,civ jet      ic,cl .150000+00 /
FI=====/
CC////////// THE END /////////////////

```

There are three types of lines in the BADA.GPF file with the line type identified by the first two characters in the line. These line types with their associated two leading characters are listed below.

**CC** comment line

**CD** data line

**FI** end-of-file line.

The data is organised into a three blocks separated by a comment line consisting of equal signs "=":

- file identification block;
- class block; and,
- parameter block

Each of these blocks is described in the subsections below.

### 6.7.1 File Identification Block

The file identification block provides information on the file name, revision number and modification date. The block consists of 11 comment lines and one data line.

```
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC  
CC /  
CC GLOBAL PARAMETERS FILE /  
CC /  
CC BADA RCS File Id /  
CC File Name Current Revision Last Modification /  
CC revision date revision date /  
CC BADA.GPF 3.0.1.1 98/03/13 3.0.1.1 98/03/13 /  
CC /  
CC BADA Revision: /  
CC /  
1-> CD Rev 3.0 /
```

The data line gives the BADA Revision Id to which the file belongs. This value is specified in the following fixed format (Fortran notation):

'CD', 8X, F3.1

The comment lines specify the file name along with the RCS current revision and last modification revision. For all released files, the current revision number and date will be the same as the number and date of the BADA Revision. The last modification revision number and date indicate when the contents of the file were last modified.

### 6.7.2 Class Block

The class block consists of 6 comment lines and defines the three classes (Flight, Engine and Phase) and their instances that are used in the BADA.GPF file.

```
CC===== Class ======/  
CC /  
CC Flight = civ,mil /  
CC Engine = jet,turbo,piston /  
CC Phase = to,ic,cl,cr,des,hold,app,lnd,gnd /  
CC /
```

With:

civ	=	civil flight
mil	=	military flight
jet	=	jet engine
turbo	=	turboprop engine
piston	=	piston engine
to	=	take off
ic	=	initial climb
cl	=	climb
cr	=	cruise
des	=	descent
hold	=	holding
app	=	approach
lnd	=	landing
gnd	=	ground

### 6.7.3 Parameter Block

The parameter block contains the values of the global aircraft parameters. This block has 5 comment lines plus a comment line and a dataline for each parameter.

```
CC===== Parameters List ======/  
CC  
CC Name      Unit  
CC Parameter  Flight   Engine    Phase          Value /  
CC  
CC max. long. acc. [fps2] /  
CD acc_long_max  civ    jet,turbo,piston to,ic,cl,cr,des,hold,app,lnd .20000E+01 /  
CC max. norm. acc. [fps2] /  
CD acc_norm_max  civ    jet,turbo,piston to,ic,cl,cr,des,hold,app,lnd .50000E+01 /  
CC nom. bank angle [deg] /  
CD ang_bank_nom  civ    jet,turbo,piston to,lnd           .15000E+02 /
```

The parameter comment line contains the parameter name and its unit.

The parameter data line contains five fields:

- (a) Parameter Field: This field identifies the parameter.
- (b) Flight Field: This field identified whether the parameter is valid for a civil flight, a military flight or both.
- (c) Engine Field: This field identifies the engine type (jet, turboprop or piston) for which the parameter is valid.
- (d) Phase Field: This field identifies for which flight phase the parameter is valid. 8 different flight phases are currently defined
- (e) Value Field: The value field gives the value of the parameter.

The fields above are specified in the following fixed format (Fortran notation):

'CD', 1X, A15, 1X, A7, 1X, A16, 1X, A29, 1X, E10.5

The parameter list continues until 'FI' (end of file) is reached.

## 7. REMOTE FILE ACCESS

All files associated with BADA Revision 3.0 are placed within a compressed tar file located on the EEC computing facilities.

This file can be accessed from a remote system using **ftp** over Internet in the following manner:

### Outside the EEC:

- (a) Initiate an **ftp** session to the Internet address: **bada.eurocontrol.fr** using the **anonymous** account. No password is needed for this account, however, to allow for tracing of access to the account it is requested that your E-mail address is used as the password, that is:

**name@machine.domain.country**

- (b) Change the working directory to **bada/3.0**:

**cd bada/3.0**

- (c) Copy the following file to your local system using the **ftp get** command:

**get bada/3.0/badaRevision3.0.tar.Z**

- (d) Uncompress the file, that is,

**uncompress badaRevision3.0.tar.Z**

- (e) Restore from the tar archive file, that is:

**tar xf badaRevision3.0.tar bada3.0**

This will restore the following files:

bada3.0/releaseSummary	
bada3.0/SYNONYM.LST	bada3.0/RCS/SYNONYM.LST,v
bada3.0/SYNONYM.NEW	bada3.0/RCS/SYNONYM.NEW,v
bada3.0/BADA.GPF	bada3.0/RCS/BADA.GPF,v
bada3.0/*.OPF	bada3.0/RCS/*.OPF,v
bada3.0/*.APF	bada3.0/RCS/*.APF,v
bada3.0/*.PTF	

Note that the \*.OPF, \*.APF, \*.PTF, BADA.GPF, SYNONYM.\* and revisionSummary files are also located in the directory and can be copied individually. A summary list of the files to be restored as obtained by using the **tar -tvf** command is provided as Appendix B.

**Inside the EEC:****from UNIX:**

- (a) Initiate an **ftp** session to the Internet address: **ftp.eurocontrol.fr** using the **anonymous** account. No password is needed for this account, however, to allow for tracing of access to the account it is requested that your E-mail address is used as the password, that is:

**name@eurocontrol.fr**

From here onwards you may follow the same procedure as for those outside the EEC.

**from PC:**

- (a) Click on the "EEC Network" icon and then click on "Wftp". Fill in:

Remote Host Name: **bada.uneec.eurocontrol.fr**

User Name: **anonymous**

Password: *your own e-mail address*

From here onwards you may follow the same procedure as for those outside the EEC.

Note that any enquiries can be addressed to the current BADA Configuration Manager at the EEC:

E-mail: **bada@eurocontrol.fr**

Phone: **+ 33 1 69 88 73 79**

Fax: **+ 33 1 69 88 73 33**

BADA web page: **<http://www.eurocontrol.fr/projects/bada/>**

## **APPENDIX A**

### **BADA 3.0 - REVISION SUMMARY FILE**

## BADA Revision Summary File

Revision Id: 3.0  
 Release Date: 98/03/12  
 Number of Files: 204

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File Name	Revision	Last Modification ( revision      date )	Size (bytes)	Checksum
SYNONYM.LST	3.0	2.6.1.5 98/03/11	9139	3321070189
SYNONYM.NEW	3.0	2.6.1.5 98/03/11	12613	3911655264
A300__.APF	3.0	2.6.1.1 98/03/11	2424	3771959147
A300__.OPF	3.0	2.6.1.1 98/03/11	4392	1648187121
A300__.PTF	3.0		5456	3603509061
A310__.APF	3.0	2.6.1.1 98/03/11	2424	3853670028
A310__.OPF	3.0	2.6.1.1 98/03/11	4392	2403247105
A310__.PTF	3.0		5456	1796598137
A320__.APF	3.0	2.6.1.1 98/03/11	2424	3383975027
A320__.OPF	3.0	2.6.1.1 98/03/11	4392	2812717343
A320__.PTF	3.0		5456	1904620621
A330__.APF	3.0	2.6.1.1 98/03/11	2424	2245963752
A330__.OPF	3.0	2.6.1.1 98/03/11	4392	2230888666
A330__.PTF	3.0		5456	1396205392
A340__.APF	3.0	2.6.1.1 98/03/11	2424	1597907885
A340__.OPF	3.0	2.6.1.1 98/03/11	4392	2672150402
A340__.PTF	3.0		5456	722113420
ATP___.APF	3.0	2.6.1.1 98/03/10	2424	1568136477
ATP___.OPF	3.0	2.6.1.1 98/03/10	4392	3783857649
ATP___.PTF	3.0		5316	2637710201
ATR___.APF	3.0	2.6.1.1 98/03/09	2424	898333471
ATR___.OPF	3.0	2.6.1.1 98/03/09	4392	1310713776
ATR___.PTF	3.0		5456	607023400
B707___.APF	3.0	2.3.1.1 95/08/29	2424	3384899920
B707___.OPF	3.0	2.6.1.1 98/03/09	4392	3475676510
B707___.PTF	3.0		5456	3363309861
B727___.APF	3.0	2.4.1.1 96/09/17	2424	848983513
B727___.OPF	3.0	2.6.1.1 98/03/09	4392	306227961
B727___.PTF	3.0		5456	1683373995
B73A___.APF	3.0	2.6.1.1 98/03/09	2424	76727621
B73A___.OPF	3.0	2.6.1.1 98/03/09	4392	2068072454
B73A___.PTF	3.0		5456	3228492830
B73B___.APF	3.0	2.6.1.1 98/03/09	2424	4093316048
B73B___.OPF	3.0	2.6.1.1 98/03/09	4392	2968537222
B73B___.PTF	3.0		5456	3289635379
B73C___.APF	3.0	2.6.1.1 98/03/10	2424	2410741838
B73C___.OPF	3.0	2.6.1.1 98/03/10	4392	370445092
B73C___.PTF	3.0		5456	69476961
B74A___.APF	3.0	2.6.1.1 98/03/10	2424	1176517015
B74A___.OPF	3.0	2.6.1.1 98/03/10	4392	2894794453

## BADA Revision Summary File

Revision Id: 3.0  
 Release Date: 98/03/12  
 Number of Files: 204

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File Name	Revision	Last Modification ( revision      date )	Size (bytes)	Checksum
B74A__.PTF	3.0		5456	4242156624
B74B__.APF	3.0	2.6.1.1 98/03/10	2424	2583143342
B74B__.OPF	3.0	2.6.1.1 98/03/10	4392	1217939273
B74B__.PTF	3.0		5456	2870255733
B757__.APF	3.0	2.6.1.1 97/10/30	2424	3454994374
B757__.OPF	3.0	2.6.1.3 98/03/10	4392	3075411763
B757__.PTF	3.0		5456	3763717021
B767__.APF	3.0	2.4.1.2 96/09/05	2424	2620952220
B767__.OPF	3.0	2.6.1.2 98/03/10	4392	4094380984
B767__.PTF	3.0		5456	2863422390
B777__.APF	3.0	2.6.1.1 97/10/30	2424	4201254410
B777__.OPF	3.0	2.6.1.2 98/03/10	4392	4257475631
B777__.PTF	3.0		5456	1463512845
BA11__.APF	3.0	2.2.1.2 95/05/18	2424	3346053700
BA11__.OPF	3.0	2.6.1.1 98/03/10	4392	1261628342
BA11__.PTF	3.0		5456	1466834918
BA46__.APF	3.0	2.4.1.2 96/10/07	2424	562223678
BA46__.OPF	3.0	2.6.1.2 98/03/10	4392	3897942505
BA46__.PTF	3.0		5456	2845656414
BADA.GPF	3.0	2.6.1.3 98/03/11	10350	1766419666
BE20__.APF	3.0	2.6.1.1 97/12/23	2424	3264013694
BE20__.OPF	3.0	2.6.1.3 98/03/10	4392	3535217046
BE20__.PTF	3.0		5456	19057551
BE99__.APF	3.0	2.4.1.1 96/02/09	2424	1059743318
BE99__.OPF	3.0	2.6.1.1 98/03/10	4392	1307417924
BE99__.PTF	3.0		5456	4222627511
BE9L__.APF	3.0	2.6.1.1 98/03/10	2424	680825676
BE9L__.OPF	3.0	2.6.1.1 98/03/10	4392	108528330
BE9L__.PTF	3.0		5436	2084762639
C130__.APF	3.0	2.2.1.1 95/03/03	2424	1857077402
C130__.OPF	3.0	2.6.1.1 98/03/10	4392	2457608933
C130__.PTF	3.0		5456	1590242801
C160__.APF	3.0	2.6.1.1 98/03/11	2424	1142812903
C160__.OPF	3.0	2.6.1.1 98/03/11	4392	866311316
C160__.PTF	3.0		5416	38722519
C421__.APF	3.0	2.3.1.1 95/12/08	2424	1976624049
C421__.OPF	3.0	2.6.1.1 98/03/10	4392	667608365
C421__.PTF	3.0		5416	2659346670
C550__.APF	3.0	2.2.1.1 95/03/03	2424	308325789
C550__.OPF	3.0	2.6.1.1 98/03/10	4392	3083724584

## BADA Revision Summary File

Revision Id: 3.0  
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File Name	Revision	Last Modification ( revision      date )	Size (bytes)	Checksum
C550__.PTF	3.0		5456	2340318936
C560__.APF	3.0	2.2.1.1 95/03/03	2424	1609139078
C560__.OPF	3.0	2.6.1.2 98/03/10	4392	812320206
C560__.PTF	3.0		5456	1487555943
CARJ__.APF	3.0	2.6.1.1 98/03/10	2424	804489421
CARJ__.OPF	3.0	2.6.1.1 98/03/10	4392	3766643145
CARJ__.PTF	3.0		5456	1103032085
CL60__.APF	3.0	2.2.1.2 95/05/18	2424	3814162316
CL60__.OPF	3.0	2.6.1.2 98/03/10	4392	798687924
CL60__.PTF	3.0		5456	3036175060
D228__.APF	3.0	2.2.1.2 95/03/03	2424	2717563115
D228__.OPF	3.0	2.6.1.1 98/03/10	4392	1017067603
D228__.PTF	3.0		5456	3105255120
D328__.APF	3.0	2.2.1.2 95/05/18	2424	3441599642
D328__.OPF	3.0	2.6.1.2 98/03/10	4392	704958531
D328__.PTF	3.0		5456	3845105803
DC10__.APF	3.0	2.2.1.1 95/03/03	2424	3983507695
DC10__.OPF	3.0	2.6.1.1 98/03/10	4392	186747372
DC10__.PTF	3.0		5456	3327183032
DC8___.APF	3.0	2.6.1.1 98/03/10	2424	2992636510
DC8___.OPF	3.0	2.6.1.1 98/03/10	4392	2440651596
DC8___.PTF	3.0		5456	4272565168
DC9___.APF	3.0	2.4.1.1 96/08/14	2424	496952227
DC9___.OPF	3.0	2.6.1.1 98/03/10	4392	1449878113
DC9___.PTF	3.0		5456	2573151330
DHC8__.APF	3.0	2.6.1.1 98/03/10	2424	815536267
DHC8__.OPF	3.0	2.6.1.1 98/03/10	4392	3503173983
DHC8__.PTF	3.0		5396	2911479696
E120__.APF	3.0	2.6.1.1 97/12/23	2424	2352537449
E120__.OPF	3.0	2.6.1.2 98/03/10	4392	1541104941
E120__.PTF	3.0		5376	741224393
F100__.APF	3.0	2.6.1.1 98/03/11	2424	1363249949
F100__.OPF	3.0	2.6.1.1 98/03/11	4392	3866386849
F100__.PTF	3.0		5456	840459740
F27___.APF	3.0	2.6.1.1 98/03/11	2424	6963559
F27___.OPF	3.0	2.6.1.1 98/03/11	4392	3707460637
F27___.PTF	3.0		5356	3082011071
F28___.APF	3.0	2.6.1.1 98/03/11	2424	1735954986
F28___.OPF	3.0	2.6.1.1 98/03/11	4392	3299691171
F28___.PTF	3.0		5456	8482661

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F50____.APF	3.0	2.6.1.1 98/03/11	2424	3603336018
F50____.OPF	3.0	2.6.1.1 98/03/11	4392	3713869555
F50____.PTF	3.0		5356	146115686
F70____.APF	3.0	2.6.1.1 98/03/11	2424	2437887281
F70____.OPF	3.0	2.6.1.1 98/03/11	4392	3177172925
F70____.PTF	3.0		5456	381191563
F900____.APF	3.0	2.6.1.1 98/03/10	2424	960975756
F900____.OPF	3.0	2.6.1.1 98/03/10	4392	2351491401
F900____.PTF	3.0		5456	2831247663
FA10____.APF	3.0	2.6.1.1 98/03/10	2424	493877130
FA10____.OPF	3.0	2.6.1.1 98/03/10	4392	2589871992
FA10____.PTF	3.0		5456	539846095
FA20____.APF	3.0	2.6.1.1 98/03/10	2424	2579510731
FA20____.OPF	3.0	2.6.1.1 98/03/10	4392	1244153771
FA20____.PTF	3.0		5456	3031235020
FA50____.APF	3.0	2.6.1.1 98/03/10	2424	1621354687
FA50____.OPF	3.0	2.6.1.1 98/03/10	4392	2632959034
FA50____.PTF	3.0		5456	3629304212
FGTR____.APF	3.0	2.2.1.2 95/05/18	2424	2373804089
FGTR____.OPF	3.0	2.6.1.1 98/03/11	4392	763867833
FGTR____.PTF	3.0		5456	566041842
H25B____.APF	3.0	2.6.1.1 98/03/11	2424	632272109
H25B____.OPF	3.0	2.6.1.1 98/03/11	4392	330887695
H25B____.PTF	3.0		5456	3083307741
JSTA____.APF	3.0	2.6.1.1 98/03/10	2424	3768576194
JSTA____.OPF	3.0	2.6.1.1 98/03/10	4392	4197954377
JSTA____.PTF	3.0		5376	819299757
JSTB____.APF	3.0	2.6.1.1 98/03/10	2424	1453021545
JSTB____.OPF	3.0	2.6.1.1 98/03/10	4392	3978602632
JSTB____.PTF	3.0		5376	3542409221
L101____.APF	3.0	2.2.1.1 95/03/03	2424	2345357063
L101____.OPF	3.0	2.6.1.1 98/03/11	4392	939462664
L101____.PTF	3.0		5456	3213944818
LJ35____.APF	3.0	2.6.1.1 98/03/11	2424	2772995920
LJ35____.OPF	3.0	2.6.1.1 98/03/11	4392	4113180257
LJ35____.PTF	3.0		5456	638163526
MD11____.APF	3.0	2.2.1.1 95/05/03	2424	932349723
MD11____.OPF	3.0	2.6.1.2 98/03/11	4392	1923736165
MD11____.PTF	3.0		5456	130693079
MD80____.APF	3.0	2.5.1.1 97/09/01	2424	43971345

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MU2__.APF	3.0	2.2.1.1 95/03/03	2424	1600031570
MU2__.OPF	3.0	2.6.1.1 98/03/11	4392	2702350542
MU2__.PTF	3.0		5456	143605460
P31T__.APF	3.0	2.6.1.1 98/03/11	2424	1958839028
P31T__.OPF	3.0	2.6.1.1 98/03/11	4392	597187425
P31T__.PTF	3.0		5456	3314579036
PA27__.APF	3.0	2.6.1.1 98/03/11	2424	2833122082
PA27__.OPF	3.0	2.6.1.1 98/03/11	4392	2558151614
PA27__.PTF	3.0		5296	2853608028
PA28__.APF	3.0	2.2.1.2 95/05/18	2424	627543673
PA28__.OPF	3.0	2.6.1.2 98/03/11	4392	3994381760
PA28__.PTF	3.0		5216	3534480572
PA31__.APF	3.0	2.2.1.1 95/03/03	2424	3826646828
PA31__.OPF	3.0	2.6.1.1 98/03/11	4392	1120025720
PA31__.PTF	3.0		5356	3722379860
PA34__.APF	3.0	2.2.1.2 95/05/18	2424	545240778
PA34__.OPF	3.0	2.6.1.1 98/03/11	4392	3248020231
PA34__.PTF	3.0		5236	3561411367
PA42__.APF	3.0	2.4.1.1 96/02/09	2424	3986842120
PA42__.OPF	3.0	2.6.1.1 98/03/11	4392	147265546
PA42__.PTF	3.0		5456	619887946
SB20__.APF	3.0	2.6.1.2 97/12/23	2424	2737866775
SB20__.OPF	3.0	2.6.1.4 98/03/11	4392	1553104317
SB20__.PTF	3.0		5456	3538268120
SF34__.APF	3.0	2.6.1.1 97/12/23	2424	76058380
SF34__.OPF	3.0	2.6.1.2 98/03/11	4392	3808836075
SF34__.PTF	3.0		5456	868601208
SH36__.APF	3.0	2.2.1.2 95/05/18	2424	2944488666
SH36__.OPF	3.0	2.6.1.1 98/03/11	4392	2066155456
SH36__.PTF	3.0		5356	1686348041
SW3__.APF	3.0	2.2.1.1 95/03/03	2424	87932188
SW3__.OPF	3.0	2.6.1.1 98/03/11	4392	3864732161
SW3__.PTF	3.0		5456	3262246856
T134__.APF	3.0	2.6.1.1 98/03/11	2424	1138962794
T134__.OPF	3.0	2.6.1.1 98/03/11	4392	367022623
T134__.PTF	3.0		5456	3853667900
T154__.APF	3.0	2.6.1.1 98/03/11	2424	4100109426
T154__.OPF	3.0	2.6.1.1 98/03/11	4392	3142849690

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TRIN__.OPF    3.0          2.6.1.1    98/03/11      4392      1225874764
TRIN__.PTF    3.0          2.6.1.1    98/03/11      5216      1270346191
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## **APPENDIX B**

### **BADA 3.0 - TAR FILE CONTENTS**

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r--r--r-- 206/201 18782 Mar 12 10:14 1998 bada3.0/RCS/MU2\_\_.OPF,v  
r--r--r-- 206/201 3328 Mar 12 10:14 1998 bada3.0/RCS/P31T\_\_.APF,v  
r--r--r-- 206/201 5213 Mar 12 10:14 1998 bada3.0/RCS/P31T\_\_.OPF,v  
r--r--r-- 206/201 3328 Mar 12 10:14 1998 bada3.0/RCS/PA27\_\_.APF,v  
r--r--r-- 206/201 5213 Mar 12 10:14 1998 bada3.0/RCS/PA27\_\_.OPF,v  
r--r--r-- 206/201 10031 Mar 12 10:14 1998 bada3.0/RCS/PA28\_\_.APF,v  
r--r--r-- 206/201 19195 Mar 12 10:14 1998 bada3.0/RCS/PA28\_\_.OPF,v  
r--r--r-- 206/201 9120 Mar 12 10:14 1998 bada3.0/RCS/PA31\_\_.APF,v  
r--r--r-- 206/201 19317 Mar 12 10:15 1998 bada3.0/RCS/PA31\_\_.OPF,v  
r--r--r-- 206/201 10030 Mar 12 10:15 1998 bada3.0/RCS/PA34\_\_.APF,v  
r--r--r-- 206/201 18943 Mar 12 10:15 1998 bada3.0/RCS/PA34\_\_.OPF,v  
r--r--r-- 206/201 10040 Mar 12 10:15 1998 bada3.0/RCS/PA42\_\_.APF,v  
r--r--r-- 206/201 19325 Mar 12 10:15 1998 bada3.0/RCS/PA42\_\_.OPF,v  
r--r--r-- 206/201 4240 Mar 12 10:15 1998 bada3.0/RCS/SB20\_\_.APF,v  
r--r--r-- 206/201 7375 Mar 12 10:15 1998 bada3.0/RCS/SB20\_\_.OPF,v  
r--r--r-- 206/201 10545 Mar 12 10:15 1998 bada3.0/RCS/SF34\_\_.APF,v  
r--r--r-- 206/201 19731 Mar 12 10:16 1998 bada3.0/RCS/SF34\_\_.OPF,v  
r--r--r-- 206/201 6556 Mar 12 10:16 1998 bada3.0/RCS/SH36\_\_.APF,v  
r--r--r-- 206/201 13895 Mar 12 10:16 1998 bada3.0/RCS/SH36\_\_.OPF,v  
r--r--r-- 206/201 9121 Mar 12 10:16 1998 bada3.0/RCS/SW3\_\_.APF,v  
r--r--r-- 206/201 19310 Mar 12 10:16 1998 bada3.0/RCS/SW3\_\_.OPF,v  
r--r--r-- 206/201 3328 Mar 12 10:16 1998 bada3.0/RCS/T134\_\_.APF,v  
r--r--r-- 206/201 5213 Mar 12 10:16 1998 bada3.0/RCS/T134\_\_.OPF,v  
r--r--r-- 206/201 3328 Mar 12 10:16 1998 bada3.0/RCS/T154\_\_.APF,v  
r--r--r-- 206/201 5214 Mar 12 10:16 1998 bada3.0/RCS/T154\_\_.OPF,v  
r--r--r-- 206/201 3328 Mar 12 10:17 1998 bada3.0/RCS/TRIN\_\_.APF,v  
r--r--r-- 206/201 5213 Mar 12 10:17 1998 bada3.0/RCS/TRIN\_\_.OPF,v  
r--rw-r-- 206/201 17668 Mar 12 10:17 1998 bada3.0/revisionSummary  
r--r--r-- 206/201 9139 Mar 12 10:01 1998 bada3.0/SYNONYM.LST  
r--r--r-- 206/201 12613 Mar 12 10:01 1998 bada3.0/SYNONYM.NEW  
r--r--r-- 206/201 2424 Mar 12 10:01 1998 bada3.0/A300\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:02 1998 bada3.0/A300\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/A300\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:02 1998 bada3.0/A310\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:02 1998 bada3.0/A310\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/A310\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:02 1998 bada3.0/A320\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:02 1998 bada3.0/A320\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/A320\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:02 1998 bada3.0/A330\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:02 1998 bada3.0/A330\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/A330\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:02 1998 bada3.0/A340\_\_.APF

r--r--r-- 206/201 4392 Mar 12 10:02 1998 bada3.0/A340\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/A340\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:02 1998 bada3.0/ATP\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:02 1998 bada3.0/ATP\_\_.OPF  
r--r--r-- 206/201 5316 Mar 12 15:03 1998 bada3.0/ATP\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:02 1998 bada3.0/ATR\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:03 1998 bada3.0/ATR\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/ATR\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:03 1998 bada3.0/B707\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:03 1998 bada3.0/B707\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B707\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:03 1998 bada3.0/B727\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:03 1998 bada3.0/B727\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B727\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:03 1998 bada3.0/B73A\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:03 1998 bada3.0/B73A\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B73A\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:03 1998 bada3.0/B73B\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:04 1998 bada3.0/B73B\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B73B\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:04 1998 bada3.0/B73C\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:04 1998 bada3.0/B73C\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B73C\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:04 1998 bada3.0/B74A\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:04 1998 bada3.0/B74A\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B74A\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:04 1998 bada3.0/B74B\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:04 1998 bada3.0/B74B\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B74B\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:04 1998 bada3.0/B757\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:04 1998 bada3.0/B757\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B757\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:04 1998 bada3.0/B767\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:05 1998 bada3.0/B767\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B767\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:05 1998 bada3.0/B777\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:05 1998 bada3.0/B777\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/B777\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:05 1998 bada3.0/BA11\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:05 1998 bada3.0/BA11\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/BA11\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:05 1998 bada3.0/BA46\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:05 1998 bada3.0/BA46\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/BA46\_\_.PTF  
r--r--r-- 206/201 10350 Mar 12 10:06 1998 bada3.0/BADA.GPF  
r--r--r-- 206/201 2424 Mar 12 10:06 1998 bada3.0/BE20\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:06 1998 bada3.0/BE20\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/BE20\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:06 1998 bada3.0/BE99\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:06 1998 bada3.0/BE99\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/BE99\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:06 1998 bada3.0/BE9L\_\_.APF

r--r--r-- 206/201 4392 Mar 12 10:06 1998 bada3.0/BE9L\_\_.OPF  
r--r--r-- 206/201 5436 Mar 12 15:03 1998 bada3.0/BE9L\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:06 1998 bada3.0/C130\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:07 1998 bada3.0/C130\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/C130\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:07 1998 bada3.0/C160\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:07 1998 bada3.0/C160\_\_.OPF  
r--r--r-- 206/201 5416 Mar 12 15:03 1998 bada3.0/C160\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:07 1998 bada3.0/C421\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:07 1998 bada3.0/C421\_\_.OPF  
r--r--r-- 206/201 5416 Mar 12 15:03 1998 bada3.0/C421\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:07 1998 bada3.0/C550\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:07 1998 bada3.0/C550\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/C550\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:07 1998 bada3.0/C560\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:08 1998 bada3.0/C560\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/C560\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:08 1998 bada3.0/CARJ\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:08 1998 bada3.0/CARJ\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/CARJ\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:08 1998 bada3.0/CL60\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:08 1998 bada3.0/CL60\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/CL60\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:08 1998 bada3.0/D228\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:08 1998 bada3.0/D228\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/D228\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:08 1998 bada3.0/D328\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:09 1998 bada3.0/D328\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/D328\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:09 1998 bada3.0/DC10\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:09 1998 bada3.0/DC10\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/DC10\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:09 1998 bada3.0/DC8\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:09 1998 bada3.0/DC8\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/DC8\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:09 1998 bada3.0/DC9\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:09 1998 bada3.0/DC9\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/DC9\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:09 1998 bada3.0/DHC8\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:09 1998 bada3.0/DHC8\_\_.OPF  
r--r--r-- 206/201 5396 Mar 12 15:03 1998 bada3.0/DHC8\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:10 1998 bada3.0/E120\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:10 1998 bada3.0/E120\_\_.OPF  
r--r--r-- 206/201 5376 Mar 12 15:03 1998 bada3.0/E120\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:10 1998 bada3.0/F100\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:10 1998 bada3.0/F100\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/F100\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:10 1998 bada3.0/F27\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:10 1998 bada3.0/F27\_\_.OPF  
r--r--r-- 206/201 5356 Mar 12 15:03 1998 bada3.0/F27\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:10 1998 bada3.0/F28\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:10 1998 bada3.0/F28\_\_.OPF

r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/F28\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:10 1998 bada3.0/F50\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:10 1998 bada3.0/F50\_\_.OPF  
r--r--r-- 206/201 5356 Mar 12 15:03 1998 bada3.0/F50\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:11 1998 bada3.0/F70\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:11 1998 bada3.0/F70\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/F70\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:11 1998 bada3.0/F900\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:11 1998 bada3.0/F900\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/F900\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:11 1998 bada3.0/FA10\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:11 1998 bada3.0/FA10\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/FA10\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:11 1998 bada3.0/FA20\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:11 1998 bada3.0/FA20\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/FA20\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:11 1998 bada3.0/FA50\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:11 1998 bada3.0/FA50\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/FA50\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:11 1998 bada3.0/FGTR\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:11 1998 bada3.0/FGTR\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/FGTR\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:12 1998 bada3.0/H25B\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:12 1998 bada3.0/H25B\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/H25B\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:12 1998 bada3.0/JSTA\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:12 1998 bada3.0/JSTA\_\_.OPF  
r--r--r-- 206/201 5376 Mar 12 15:03 1998 bada3.0/JSTA\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:12 1998 bada3.0/JSTB\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:12 1998 bada3.0/JSTB\_\_.OPF  
r--r--r-- 206/201 5376 Mar 12 15:03 1998 bada3.0/JSTB\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:12 1998 bada3.0/L101\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:12 1998 bada3.0/L101\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/L101\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:12 1998 bada3.0/LJ35\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:12 1998 bada3.0/LJ35\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/LJ35\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:13 1998 bada3.0/MD11\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:13 1998 bada3.0/MD11\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/MD11\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:13 1998 bada3.0/MD80\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:13 1998 bada3.0/MD80\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/MD80\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:13 1998 bada3.0/MU2\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:14 1998 bada3.0/MU2\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/MU2\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:14 1998 bada3.0/P31T\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:14 1998 bada3.0/P31T\_\_.OPF  
r--r--r-- 206/201 5456 Mar 12 15:03 1998 bada3.0/P31T\_\_.PTF  
r--r--r-- 206/201 2424 Mar 12 10:14 1998 bada3.0/PA27\_\_.APF  
r--r--r-- 206/201 4392 Mar 12 10:14 1998 bada3.0/PA27\_\_.OPF  
r--r--r-- 206/201 5296 Mar 12 15:03 1998 bada3.0/PA27\_\_.PTF

r--r--- 206/201 2424 Mar 12 10:14 1998 bada3.0/PA28\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:14 1998 bada3.0/PA28\_\_.OPF  
r--r--- 206/201 5216 Mar 12 15:03 1998 bada3.0/PA28\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:14 1998 bada3.0/PA31\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:15 1998 bada3.0/PA31\_\_.OPF  
r--r--- 206/201 5356 Mar 12 15:03 1998 bada3.0/PA31\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:15 1998 bada3.0/PA34\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:15 1998 bada3.0/PA34\_\_.OPF  
r--r--- 206/201 5236 Mar 12 15:03 1998 bada3.0/PA34\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:15 1998 bada3.0/PA42\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:15 1998 bada3.0/PA42\_\_.OPF  
r--r--- 206/201 5456 Mar 12 15:03 1998 bada3.0/PA42\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:15 1998 bada3.0/SB20\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:15 1998 bada3.0/SB20\_\_.OPF  
r--r--- 206/201 5456 Mar 12 15:03 1998 bada3.0/SB20\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:15 1998 bada3.0/SF34\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:16 1998 bada3.0/SF34\_\_.OPF  
r--r--- 206/201 5456 Mar 12 15:03 1998 bada3.0/SF34\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:16 1998 bada3.0/SH36\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:16 1998 bada3.0/SH36\_\_.OPF  
r--r--- 206/201 5356 Mar 12 15:03 1998 bada3.0/SH36\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:16 1998 bada3.0/SW3\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:16 1998 bada3.0/SW3\_\_.OPF  
r--r--- 206/201 5456 Mar 12 15:03 1998 bada3.0/SW3\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:16 1998 bada3.0/T134\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:16 1998 bada3.0/T134\_\_.OPF  
r--r--- 206/201 5456 Mar 12 15:03 1998 bada3.0/T134\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:16 1998 bada3.0/T154\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:16 1998 bada3.0/T154\_\_.OPF  
r--r--- 206/201 5456 Mar 12 15:03 1998 bada3.0/T154\_\_.PTF  
r--r--- 206/201 2424 Mar 12 10:17 1998 bada3.0/TRIN\_\_.APF  
r--r--- 206/201 4392 Mar 12 10:17 1998 bada3.0/TRIN\_\_.OPF  
r--r--- 206/201 5216 Mar 12 15:03 1998 bada3.0/TRIN\_\_.PTF

## **APPENDIX C**

### **BADA 3.0 - LIST OF AVAILABLE AIRCRAFT MODELS**

### List of Aircraft Types Supported by BADA 3.0

A/C Code	Model Type	Aircraft Name	Equiv. A/C	Max Alt [feet]	Wake Cat.
A10	equiv	Thunderbolt II	FGTR	50000	M
A300	direct	Airbus A300		39000	H
A310	direct	Airbus A310		41000	H
A320	direct	Airbus A320		39000	M
A330	direct	Airbus A330		41000	H
A340	direct	Airbus A340		41000	H
A4	equiv	Skyhawk	FGTR	50000	M
A6	equiv	Intruder	FGTR	50000	M
AC6T	equiv.	Rockwell Turbo Commander 690C	BE20	32000	L
AN12	equiv	Antonov AN-12	C130	30000	M
AN24	equiv	Antonov AN-24	F27	25000	M
AN26	equiv	Antonov AN-26	F27	25000	M
ATP	direct	BAe Advanced Turboprop		25000	M
ATR	direct	ATR 42 / 72		25000	M
B190	equiv	Beech 1900	JSTA	25000	L
B707	direct	Boeing 707-300/400 series		42000	M
B720	equiv	Boeing 720B	B707	42000	M
B727	direct	Boeing 727, all series		37000	M
B73A	direct	Boeing 737-100/200 series		37000	M
B73B	direct	Boeing 737-300/400/500 series		37000	M
B73C	direct	Boeing 737-600/700/800 series		45000	M
B74A	direct	Boeing 747-100/200/300 series		45000	H
B74B	direct	Boeing 747-400		45000	H
B74S	equiv.	Boeing 747 SP	B74B	45000	H
B757	direct	Boeing 757 all series		42000	M
B767	direct	Boeing 767 all series		42000	H
B777	direct	Boeing 777 all series		43100	H
BA11	direct	BAe 111, all series		35000	M

BA46	direct	BAe 146-100/200/300		33000	M
BE20	direct	Beech Super King Air 200 / Huron		32000	L
BE30	equiv.	Beech Super King Air 300	BE20	32000	L
BE33	equiv	Beech Bonanza 33	PA34	15000	L
BE36	equiv	Beech Bonanza 36	PA34	15000	L
BE58	equiv	Beech Baron 58	PA27	20000	L
BE60	equiv	Beech Duke 60	C421	23500	L
BE95	equiv.	Beech Travelair 95	PA31	23000	L
BE99	direct	Beech Airliner C99		15000	L
BE9L	direct	Beech King Air 90		31000	L
BN2P	equiv.	Pilatus Islander BN2-A/B	PA31	23000	L
C130	direct	Lockheed Hercules		40000	M
C135	equiv.	Boeing Stratolifter 717	B707	42000	M
C141	equiv	Lockheed Starlifter	DC8	42000	H
C160	direct	Aerospatiale Transall C160		30000	M
C172	equiv.	Cessna Skyhawk 172	PA28	12000	L
C177	equiv.	Cessna Cardinal 177	PA28	12000	L
C182	equiv.	Cessna Skylane 182	PA28	12000	L
C303	equiv	Cessna Crusader 303	PA31	23500	L
C310	equiv	Cessna 310/310T	PA31	23000	L
C340	equiv.	Cessna 340/340A	PA31	23000	L
C402	equiv.	Cessna 402	PA31	23000	L
C414	equiv	Cessna Chancellor 414	C421	23500	L
C421	direct	Cessna Golden Eagle 421		23500	L
C425	equiv	Cessna Corsair/Conquest	P31T	29000	L
C5	equiv	Lockheed Galaxy	B74A	40000	H
C500	equiv.	Cessna Citation	C550	43000	L
C525	equiv	Cessna Citationjet 525	C550	43000	L
C550	direct	Cessna Citation II-S2		43000	L
C560	direct	Cessna Citation V		45000	M
C650	equiv.	Cessna Citation III	LJ35	43000	M

CARJ	direct	Canadair Regional Jet		41000	M
CL60	direct	Canadair Challenger 600/601		41000	M
CN35	equiv	Airtech (CASA/IPTN) CN-235	ATR	25000	M
CONC	equiv	BAe-Aerospatiale Concorde	FGTR	50000	H
CVLT	equiv	Convair 580	ATR	25000	M
D228	direct	Dornier 228-100/200		29600	L
D28D	equiv.	Dornier DO 28	PA31	23000	L
D328	direct	Dornier 328		32800	M
DC10	direct	McDonnell-Douglas DC-10		39000	H
DC8	equiv.	McDonnell-Douglas DC-8 all series	DC8	42000	H
DC9	direct	McDonnell-Douglas DC-9		35000	M
DHC8	direct	De Havilland Dash 8 all series		25000	M
E110	equiv	Embrear Bandeirante	D228	29600	L
E120	direct	Embraer EMB-120 Brasilia		32000	L
E3	equiv	Boeing E-3A Sentry	B707	42000	M
F100	direct	Fokker 100		35000	M
F14	equiv	Grumman F-14 Tomcat	FGTR	50000	M
F15	equiv.	McDonnell-Douglas F15 Eagle	FGTR	50000	M
F16	equiv	General Dynamics F16 Fighting Falcon	FGTR	50000	M
F18	equiv.	McDonnell-Douglas F18 Hornet	FGTR	50000	M
F27	direct	Fokker Friendship F27		25000	M
F28	direct	Fokker Fellowship F28		35000	M
F4	equiv	McDonnell-Douglas F4 Phantom	FGTR	50000	M
F50	direct	Fokker 50		25000	M
F70	direct	Fokker 70		37000	M
F900	direct	Dassault Falcon 900		49000	M
FA10	direct	Dassault Falcon 10		45000	M
FA20	direct	Dassault Falcon 20		42000	M
FA50	direct	Dassault Falcon 50		43000	M
FGTR	direct	Generic Military Fighter		50000	M
GULF	equiv.	Gulfstream II, III, IV	CL60	41000	M

H25B	direct	BAe Dominie		41000	M
HAR	equiv.	BAe Harrier	FGTR	50000	M
IL18	equiv.	Ilyushin IL-18	C130	30000	M
IL62	equiv.	Ilyushin IL-62	B707	42000	M
IL76	equiv.	Ilyushin IL-76	A300	42000	H
IL86	equiv.	Ilyushin IL-86	DC8	42000	H
JAGR	equiv.	BAe Jaguar	FGTR	50000	M
JSTA	direct	BAe Jetstream 31		25000	L
JSTB	direct	BAe Jetstream 41		26000	L
L101	direct	Lockheed L-1011 Tristar		42000	H
L188	equiv.	Lockheed Electra/Orion	C130	30000	H
L29A	equiv	Lockheed Jetstar	CL60	41000	M
L410	equiv	LET 410	D228	29600	L
LJ31	equiv	Gates Learjet 31	LJ35	43000	M
LJ35	direct	Gates Learjet 35/36		43000	M
LR55	equiv.	Gates Learjet 55	LJ35	43000	M
M20	equiv	Mooney Mark 20	TRIN	12000	L
MD11	direct	McDonnell-Douglas MD-11		43000	H
MD80	direct	McDonnell-Douglas MD-80		37000	M
MD90	direct	McDonnell-Douglas MD-90	MD80	37000	M
MG21	equiv	Mikoyan MiG 21	FGTR	50000	M
MG23	equiv	Mikoyan MiG 23	FGTR	50000	M
MG25	equiv	Mikoyan MiG 25	FGTR	50000	M
MG29	equiv	Mikoyan MiG 29	FGTR	50000	M
MIR2	equiv	Dassault-Breguet Mirage 2000	FGTR	50000	M
MIR4	equiv.	Dassault-Breguet Mirage IV	FGTR	50000	M
MRF1	equiv	Dassault Mirage F1	FGTR	50000	M
MU2	direct	Mitsubishi Marquise/Solitaire		28000	L
MU30	equiv	Mitsubishi MU-300	C550	43000	L
P28R	equiv.	Piper Cherokee Arrow IV	TRIN	12000	L
P3	equiv.	Lockheed Orion	C130	30000	M

P31T	direct	Piper Cheyenne I/II		29000	L
PA23	equiv.	Piper Apache	PA27	20000	L
PA27	direct	Piper Aztec		20000	L
PA28	direct	Piper Cherokee Archer/Dakota		12000	L
PA31	direct	Piper Chieftain/Mojave/Navaho		23000	L
PA34	direct	PA34-200T Seneca-3		15000	L
PA42	direct	Piper Cheyenne II/IV		33000	L
S601	equiv	Aerospatiale SN601 Corvette	C550	43000	L
SB20	direct	SAAB 2000		31000	M
SB32	equiv	SAAB Lansen	FGTR	50000	M
SB35	equiv	SAAB Draken	FGTR	50000	M
SB37	equiv	SAAB Viggen	FGTR	50000	M
SB39	equiv	SAAB Gripen	FGTR	50000	M
SBR1	equiv	Rockwell Sabreliner 265	FA20	42000	M
SF34	direct	SAAB Fairchild 340		31000	M
SH33	equiv	Shorts 330	SH36	20000	M
SH36	direct	Shorts 360		20000	M
SK60	equiv	SAAB 105	FGTR	50000	M
SW2	equiv.	Fairchild Merlin IIA/B, IIIB/C, IVA	SW3	31000	L
SW3	direct	Fairchild Merlin IVC / Metro III		31000	L
SW4	equiv	Merlin II/A	SW3	31000	L
T134	direct	Tupolev TU-134		39000	M
T154	direct	Tupolev TU-154		41000	M
TOBA	equiv.	Aerospatiale Tobago TB-10	PA28	12000	L
TOR	equiv.	Panavia Tornado	FGTR	50000	M
TRIN	direct	Aerospatiale Trinidad TB-20		12000	L
VC10	equiv.	BAe VC10-1100	B707	42000	M
WW24	equiv	IAI 1124 Westwind	H25B	41000	M
YK40	equiv	Yakolev YK-40	DHC8	25000	M
YK42	equiv	Yakolev YK-42	BA46	33000	M